

SEXTUPOLE CONFIGURATIONS FOR HIGH RESOLUTION BEAM M6

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I. Introduction

High momentum resolution is a primary criterion by which the meson laboratory beam M6 is designed. It is a three-stage beam with a momentum defining slit at the end of the first stage. The dispersion is maximum at this point to give good resolution. The beam may be made essentially monochromatic by stopping down a slit located here. Recombination is done in the second and third stages with moderately high dispersion at the end of the second stage. For a larger momentum band pass, momentum determination may be done by placing counters at this point. Further description of the beam line and its potential uses may be found elsewhere.^{1,2}

The minimum momentum interval carried by the beam will be 0.03% of the central momentum. This figure also then represents the maximum momentum resolution obtainable. However the beam line can transmit a total momentum interval of 2% of the central momentum. To maximize the analyzing power of any experiment utilizing the beam, it is desirable to have this resolution capability for the entire momentum interval carried by the beam. One therefore must eliminate aberrations which cause variation of the spot size at the momentum focus with either momentum or initial angle.



In Section II below we describe the principal aberrations inherent in the design of the beam. Sections III and IV present schemes for eliminating some of these aberrations to second order. Finally in Section V we examine each of the solutions including the effect of higher order terms.

II. The Beam and Principal Aberrations

A. Basic Beam Geometry

Each of the three stages of the beam contains two quadrupole doublets. The first focuses from point to parallel, while the second refocuses the beam to a point. For both doublets the horizontally defocusing quad is placed nearer the focus. This both maximizes the resolution and helps match the beam profile with the bending magnet apertures. Between the doublets, in the parallel region, are placed the bending magnets whose purpose is either to disperse or recombine the beam in momentum. At high energies with zero gradient bending magnets, we may, for purposes of this discussion, safely ignore the focusing properties of the bending magnets. At each focus is placed a field lens quadrupole which further aids in obtaining complete momentum recombination.

For a doublet focusing point to parallel, as shown in Figure 1, two principal planes are relevant.³ The figure is drawn with the horizontally defocusing quadrupole nearer the focus, as is the case in beam line M6. If λ is the distance from the focus to the first quadrupoles, s is the distance between the centers of the quadrupoles, and f_1 and f_2 are their respective focal lengths, then in a thin lens approximation

we have:

$$f_1 = \ell \sqrt{s/(\ell + s)} \quad (1)$$

$$f_2 = \sqrt{s(\ell + s)}$$

The distances from the focus to the horizontal and vertical principal planes respectively are:

$$h_x = \ell + s + f_2 \quad (2)$$

$$h_y = \ell + s - f_2$$

The magnitude of the sine-like ray in each plane in the parallel section is equal to the distance from the focus to the corresponding principal plane.

B. Principal Aberrations

At high energies the important aberrations occurring in a beam line arise from three sources:⁴ chromatic aberrations from the quadrupoles, the effect of particles traversing a bending magnet at an angle to the central ray, and the influence of sextupoles. Since in this beam the bending magnets are placed in the parallel sections we may safely ignore the second item. We will now concentrate our attention on the chromatic aberrations of the quadrupoles.

The principal impediment to achieving high resolution over the entire momentum band carried by the beam is the variation with momentum of the focusing strength of the quads. For a point-to-point image this variation is measured by the second-order matrix elements T_{126} and T_{346} . For this case Brown⁴ has shown that the matrix element T_{126} is given by:

$$T_{126} = M_x \int_0^2 s'_x^2 dz \quad (3)$$

where M_x is the horizontal magnification and s'_x the slope of the horizontal sine-like ray. The integral is taken over the entire distance between foci. The term T_{346} may be evaluated similarly.

We now depict in Figure 2 a section of the beam, with principal planes shown for each doublet. For a thin lens approximation it may be shown that

$$T_{126} = 2(h_2 + h_3) \quad (4)$$

$$T_{346} = 2(h_1 + h_4)$$

An exact numerical calculation shows that for NAL beams this result should be accurate to within a few percent. For the optical mode used in beam line M6 the chromatic aberration will clearly be significantly greater in the horizontal than in the vertical plane.

For a two-stage beam the chromatic aberration of each stage will be affected by the magnification of the other, but the result for each stage is unchanged.

III. Two Sextupole Solution

We now address ourselves to the problem of eliminating chromatic aberration at the end of the second section.⁵ First we consider a solution which reduces the term T_{126} to zero but ignores the effect on T_{346} . As shown in the previous section chromatic aberration is larger in the horizontal plane. It is also in the horizontal plane that chromatic aberration affects the momentum resolution.

In Figure 3 we designate the positions of four sextupoles placed in the second stage of the beam, labeling them with the letters a, b, c, and d. The sextupoles straddle the doublets in pairs, sextupoles a and d being as close to the quadrupoles as possible. The dispersion ray d_x is also shown, with its crossover in the vicinity of sextupole c. In this section we consider the use of only sextupoles b and c. A solution using all four sextupoles will be discussed in Section IV.

A sextupole placed in a beam line to correct for chromatic aberrations will introduce geometric aberrations. The principal ones affecting beam spot size in this beam are T_{122} and T_{144} . Therefore we must include at least two sextupoles so their contributions to geometric terms will cancel while eliminating chromatic terms.

The changes in the relevant matrix elements due to a single sextupole are:⁴

$$\Delta T_{122} = M_x s_x^3 S \quad (5)$$

$$\Delta T_{144} = -M_x s_x s_y^2 S$$

$$\Delta T_{126} = 2M_x s_x^2 d_x S$$

where M_x is the horizontal magnification, s_x and s_y are the sine-like rays in each plane and d_x is the dispersion ray. The quantity S is a measure of the strength of the sextupole and is equal to $qBl/a^2 p_0$, where B is the pole tip field, a the half aperture, and l the length of the sextupole, and q and p_0 represent the charge and central momentum of the particles.

Since the sextupoles are both placed in the parallel section the two sine-like rays s_x and s_y have the same magnitude

for each of them. Hence by setting their strengths to be equal and opposite we may cancel the contributions to T_{122} and T_{144} .

Letting $S = S_b = -S_c$ we can eliminate the T_{126} term by setting:

$$2M_x s_{xb}^2 S (d_{xb} - d_{xc}) = -T_{126} \quad (6)$$

Actual determination of the sextupole strengths was done using the program TRANSPORT.^{6,7} Using sextupoles which are 2.5 feet long and have a half aperture of 5 cm, a pole tip field of 2.774 kilogauss is required.

IV. Four Sextupole Solution

To eliminate chromatic aberration to second order in both planes, four sextupoles are required. In addition to the chromatic term T_{346} , the geometric term T_{324} now becomes important. The coupling of a sextupole to these additional terms is given by:

$$\Delta T_{324} = -2M_y s_x s_y^2 S \quad (7)$$

$$\Delta T_{346} = -2M_y s_y^2 d_x S$$

where now s_y is the vertical sine-like ray and M_y is the vertical magnification. We see that the difference in coupling to the terms T_{144} and T_{324} lies only in the magnification term, which is a property of the entire beam line and is therefore the same for all sextupoles. Therefore if the sextupoles are set so that T_{144} is equal to zero, then T_{324} will also equal zero. We now have four terms to eliminate with four sextupoles. It remains to determine if the four couplings are sufficiently independent to guarantee that the solution will result in reasonable pole tip fields.

We may now write the equation to be solved in the form:

$$MS + T = 0 \quad (8)$$

where S is a vector giving the four sextupole strengths, T a vector made up of the uncorrected second order terms T_{122} , T_{144} , T_{126} , T_{346} respectively, and M is a matrix of the coupling terms. The uncorrected T matrix terms are those which occur when no sextupoles are included. The element M_{11} of this matrix, for example will have the form $M_x s_{xa}^3$, where s_{xa} is the magnitude of the horizontal sine-like ray at point a. By defining a new vector \bar{T} as a renormalized T whose elements are given as:

$$\bar{T} = \begin{pmatrix} T_{122}/M_x \\ -T_{144}/M_x \\ T_{126}/2M_x \\ -T_{346}/2M_y \end{pmatrix} \quad (9)$$

we may introduce a simpler Matrix \bar{M} and rewrite equation (8) as:

$$\bar{M}S + \bar{T} = 0 \quad (8a)$$

where now exhibit \bar{M} explicitly as:

$$\bar{M} = \begin{pmatrix} s_{xa}^3 & s_{xb}^3 & s_{xc}^3 & s_{xd}^3 \\ s_{xa} s_{ya}^2 & s_{xb} s_{yb}^2 & s_{xc} s_{yc}^2 & s_{xd} s_{yd}^2 \\ s_{xa}^2 d_{xa} & s_{xb}^2 d_{xb} & s_{xc}^2 d_{xc} & s_{xd}^2 d_{xd} \\ s_{ya}^2 d_{xa} & s_{yb}^2 d_{xb} & s_{yc}^2 d_{xc} & s_{yd}^2 d_{xd} \end{pmatrix} \quad (10)$$

and label the submatrices as follows:

$$\bar{M} = \begin{pmatrix} M_{11} & M_{12} U \\ M_{21} & M_{22} U \end{pmatrix} \quad (10a)$$

where the matrix U, given by:

$$U = \begin{pmatrix} 0 & 1 \\ 1 & 0 \end{pmatrix} \quad (11)$$

functions simply to interchange the columns of the matrix that multiplies it. With this definition, if the second stage of the beam were symmetric, so that the two doublets were mirror images of each other, we would have $M_{11} = M_{12}$.

Now if the matrix \bar{M} is non-singular a solution will exist. Roughly, we may say that if the determinant of \bar{M} is large, the resulting sextupole strengths will be small. Consider first the situation which would occur if the momentum recombination were done entirely in the second stage. Then we would have $d_{xc} = d_{xd} = 0$ and therefore $M_{22} = 0$. This would give us $\det(\bar{M}) = -\det(M_{12}) \cdot \det(M_{21})$, so by examining the structure of the submatrices we can gain understanding of the entire problem.

From the locations of the principal planes we see that:

$$\begin{aligned}s_{xa} &< s_{xb} \\ s_{ya} &> s_{yb} \\ s_{xd} &< s_{xc} \\ s_{yd} &> s_{yc}\end{aligned}\tag{12}$$

Examination of the coupling terms shows that sextupoles b and c will couple most strongly to T_{122} and T_{126} while sextupoles a and d couple more strongly to T_{144} and T_{346} . In essence what we are doing is first to correct T_{126} and T_{346} with sextupoles b and a respectively. Then we correct the resultant T_{122} and T_{144} terms with sextupoles c and d respectively. Examining the determinants of the submatrices and referring to equations (12) we find:

$$-\det(M_{12}) = s_{xc}^2 s_{xd}^2 (s_{xc}^2 s_{yd}^2 - s_{yc}^2 s_{xd}^2) > 0 \quad (13)$$

$$\det(M_{21}) = d_{xa}^2 d_{xb}^2 (s_{xa}^2 s_{yb}^2 - s_{ya}^2 s_{xb}^2) > 0$$

If we now define the two component vectors \bar{T}_1 and \bar{T}_2 as giving the upper and lower (geometric and chromatic) parts of \bar{T} and S_1 and S_2 as:

$$S_1 = \begin{pmatrix} s_a \\ s_b \end{pmatrix} \quad S_2 = \begin{pmatrix} s_d \\ s_c \end{pmatrix} \quad (14)$$

As explained in Section II, the components of \bar{T}_1 will be zero so we arrive at the solution:

$$S_1 = -M_{21}^{-1} \bar{T}_2 \quad (15)$$

$$S_2 = -M_{12}^{-1} M_{11} S_1$$

Now, of course, momentum recombination is not all accomplished in the second stage and the conditions $d_{xc} = 0$ and $d_{xd} = 0$ cannot simultaneously be true. However if we adjust the field lens to place the momentum crossover in the region of sextupole c, then the situation should not differ too greatly from the previous case and solution should still be possible. We must now solve the simultaneous equations:

$$M_{11} S_1 + M_{12} S_2 = 0 \quad (16)$$

$$M_{21} S_1 + M_{22} S_2 = -\bar{T}_2$$

We define a new two-component vector X as:

$$X = M_{11} S_1 . \quad (17)$$

The arguments used above to show M_{12} to be non-singular apply also to M_{11} and from the first of equations (16) we get:

$$s_1 = M_{11}^{-1}x \quad (18)$$

$$s_2 = -M_{12}^{-1}x$$

Substituting into the second of equations (16) gives:

$$(M_{21}M_{11}^{-1} - M_{22}M_{12}^{-1})x = -\bar{T}_2 \quad (19)$$

Each of the submatrices M_{11} , M_{12} , M_{21} , and M_{22} is factorizable and, for example, we have:

$$M_{11} = \begin{pmatrix} 2 & 2 \\ s_{xa} & s_{xb} \\ 2 & 2 \\ s_{ya} & s_{yb} \end{pmatrix} \begin{pmatrix} s_{xa} & 0 \\ 0 & s_{xb} \end{pmatrix} \quad (20)$$

$$M_{21} = \begin{pmatrix} 2 & 2 \\ s_{xa} & s_{xb} \\ 2 & 2 \\ s_{ya} & s_{yb} \end{pmatrix} \begin{pmatrix} d_{xa} & 0 \\ 0 & d_{xb} \end{pmatrix}$$

The first matrix on the right side is the same in each equation so that in equation (19) we have:

$$M_{21}M_{11}^{-1} - M_{22}M_{12}^{-1} = \begin{pmatrix} \frac{d_{xa}}{s_{xa}} - \frac{d_{xd}}{s_{xd}} & 0 \\ 0 & \frac{d_{xb}}{s_{xb}} - \frac{d_{xc}}{s_{xc}} \end{pmatrix}$$

Since $s_{xb} = s_{xc}$, the lower right term is $(d_{xb} - d_{xc})/s_{xb}$, indicating that here, just as for the two sextupole case, only the difference in the magnitude of the dispersion ray at the two points is important. Also by setting the momentum crossover point at sextupole c, we see that d_{xd} will be negative. Thus

we are insured that both terms are non-zero, and a solution is indeed possible. Numerical values were once again obtained with the program TRANSPORT. For sextupoles with dimensions as before, we get pole tip fields as shown:

| <u>Sextupole</u> | <u>Pole Tip Field</u> |
|------------------|-----------------------|
| s_a | -3.053 kg |
| s_b | 7.203 kg |
| s_c | -6.829 kg |
| s_d | 2.750 kg |

V. Higher Order Effects

Both the two- and the four-sextupole solutions work perfectly to second order. The obvious question, of course, is the influence of higher order effects. Such effects were examined with the use of the program TURTLE,⁸ and the resulting histograms are shown in Figures 4-17. Both horizontal and vertical planes are shown at both second and third foci. The solutions described minimize the second order terms at the second focus. The effect on the beam spot at the third focus is of interest since that is the position at the final target. All runs were made using the recombined mode of the beam as adapted to the needs of experiment no. 96.

In Figure 4 are shown respectively the vertical and horizontal beam profiles at the second focus, using the central design momentum and no sextupoles. The horizontal and vertical spots respectively at the third focus for the same beam configuration are shown in Figure 5. These profiles represent essentially

the first order beam spot. The aim of introducing correcting elements is to make the off-momentum profiles appear essentially the same.

In Figures 6 and 7 are shown the same set of profiles for a momentum one-half percent above the design central momentum. Figures 8 and 9 are the same for a momentum 1% above the design central momentum. All cases are with no sextupoles. As we get away from the central momentum all profiles begin to broaden due to chromatic aberration. As explained in Section II, the broadening in the vertical plane is substantially less than in the horizontal plane.

In Figures 10-15 we see repeated the same set of profiles, but with the two sextupole solution. We are correcting for chromatic aberration on the horizontal plane at the second focus. As can be seen, the horizontal profile at the second focus is now essentially the same for all momenta. A tail, due to higher order effects, appears, even in the on-momentum profile, but is negligible. In the horizontal plane at the third focus the chromatic aberration is greatly reduced. Some deterioration of the beam profile in the vertical plane at both foci is observed. However, if we examine the coupling terms of the sextupoles to the vertical aberrations, we discover that, with the beam geometry used, they are much smaller than those for the horizontal aberrations. Therefore the loss in the vertical plane is not nearly as great as the gain in the horizontal.

The profiles for the four sextupole solution are shown in Figures 16 and 17 for only the central momentum. The higher order terms due to coupling of sextupoles produce a substantial deterioration of the horizontal beam spot, at both second and third foci. This deterioration is, for a large fraction of the momentum band, at least as great as the effect being corrected. It cannot therefore be used as a practical solution. The conclusion is that, for this beam, one must be satisfied correcting in only the horizontal plane and accepting a small deterioration in the vertical.

References

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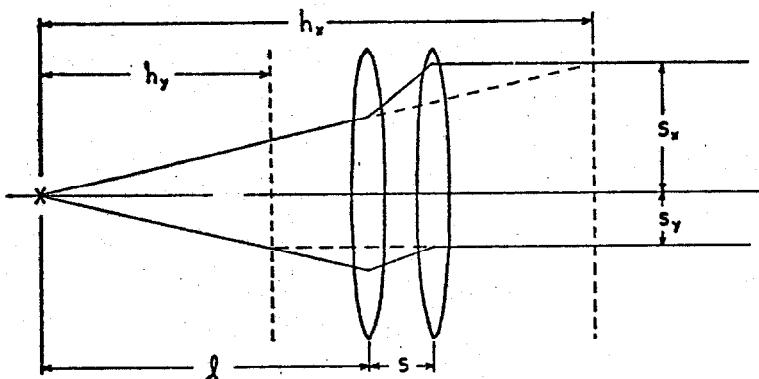


Figure 1. Doublet focusing point to parallel. The horizontally defocusing quadrupole is nearer the focus. Principal planes and sine-like rays are shown in the horizontal (x) and vertical (y) planes.

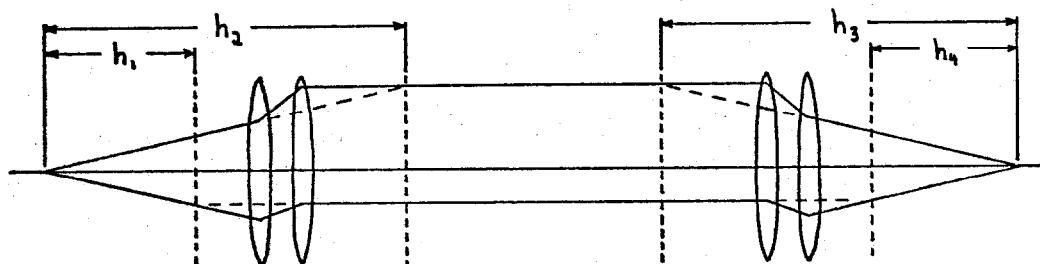


Figure 2. A section of beam line M6 omitting bending magnets. Principal planes are shown for each doublet. Sine-like rays in both planes are also included.

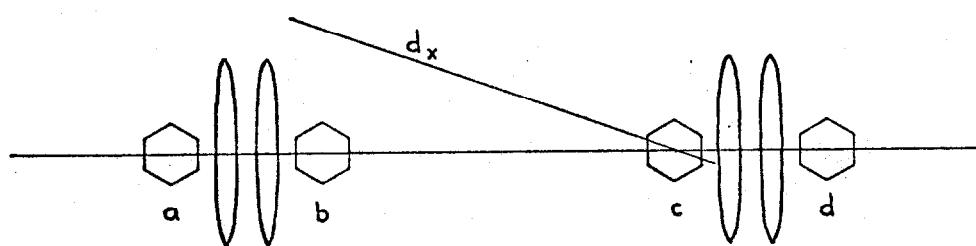


Figure 3. Second stage of beam line M6. Positions of four sextupoles a, b, c, and d are shown. The dispersion ray d_x is drawn in.

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5000 RAYS

Recombined - no sexts

(1)

-16-

$\Delta p/p = 0$

TM-374

2254.000

INTERVAL

SCALE FACTOR: 100 X'S EQUAL 328 RAYS

| LESS THAN | -0.200 | 0 |
|------------------|--------|-----|
| -0.200 TO -0.190 | -0.190 | 0 |
| -0.190 TO -0.180 | -0.180 | 0 |
| -0.180 TO -0.170 | -0.170 | 0 |
| -0.170 TO -0.160 | -0.160 | 0 |
| -0.160 TO -0.150 | -0.150 | 2 |
| -0.150 TO -0.140 | -0.140 | 5 |
| -0.140 TO -0.130 | -0.130 | 2 |
| -0.130 TO -0.120 | -0.120 | 0 |
| -0.120 TO -0.110 | -0.110 | 0 |
| -0.110 TO -0.100 | -0.100 | 41 |
| -0.100 TO -0.090 | -0.090 | 125 |
| -0.090 TO -0.080 | -0.080 | 185 |
| -0.080 TO -0.070 | -0.070 | 235 |
| -0.070 TO -0.060 | -0.060 | 262 |
| -0.060 TO -0.050 | -0.050 | 234 |
| -0.050 TO -0.040 | -0.040 | 262 |
| -0.040 TO -0.030 | -0.030 | 265 |
| -0.030 TO -0.020 | -0.020 | 318 |
| -0.020 TO -0.010 | -0.010 | 291 |
| -0.010 TO 0.000 | 0.000 | 317 |
| 0.000 TO 0.010 | 0.010 | 282 |
| 0.010 TO 0.020 | 0.020 | 341 |
| 0.020 TO 0.030 | 0.030 | 240 |
| 0.030 TO 0.040 | 0.040 | 254 |
| 0.040 TO 0.050 | 0.050 | 235 |
| 0.050 TO 0.060 | 0.060 | 245 |
| 0.060 TO 0.070 | 0.070 | 218 |
| 0.070 TO 0.080 | 0.080 | 158 |
| 0.080 TO 0.090 | 0.090 | 136 |
| 0.090 TO 0.100 | 0.100 | 35 |
| 0.100 TO 0.110 | 0.110 | 0 |
| 0.110 TO 0.120 | 0.120 | 0 |
| 0.120 TO 0.130 | 0.130 | 0 |
| 0.130 TO 0.140 | 0.140 | 2 |
| 0.140 TO 0.150 | 0.150 | 0 |
| 0.150 TO 0.160 | 0.160 | 0 |
| 0.160 TO 0.170 | 0.170 | 0 |
| 0.170 TO 0.180 | 0.180 | 2 |
| 0.180 TO 0.190 | 0.190 | 0 |
| 0.190 TO 0.200 | 0.200 | 2 |
| GREATER THAN | 0.200 | 0 |

NO 1 OF Y IN CM 1227.139 FT FROM THE TARGET

THE FOLLOWING IS A HISTOGRAM OF X FOR 5000 RAYS

(2)

INTERVAL

SCALE FACTOR: 100 X'S EQUAL 442 RAYS

| LESS THAN | -0.200 | 0 |
|------------------|--------|-----|
| -0.200 TO -0.190 | -0.190 | 0 |
| -0.190 TO -0.180 | -0.180 | 0 |
| -0.180 TO -0.170 | -0.170 | 0 |
| -0.170 TO -0.160 | -0.160 | 1 |
| -0.160 TO -0.150 | -0.150 | 0 |
| -0.150 TO -0.140 | -0.140 | 0 |
| -0.140 TO -0.130 | -0.130 | 3 |
| -0.130 TO -0.120 | -0.120 | 0 |
| -0.120 TO -0.110 | -0.110 | 0 |
| -0.110 TO -0.100 | -0.100 | 3 |
| -0.100 TO -0.090 | -0.090 | 0 |
| -0.090 TO -0.080 | -0.080 | 0 |
| -0.080 TO -0.070 | -0.070 | 117 |
| -0.070 TO -0.060 | -0.060 | 273 |
| -0.060 TO -0.050 | -0.050 | 294 |
| -0.050 TO -0.040 | -0.040 | 323 |
| -0.040 TO -0.030 | -0.030 | 361 |
| -0.030 TO -0.020 | -0.020 | 392 |
| -0.020 TO -0.010 | -0.010 | 442 |
| -0.010 TO 0.000 | 0.000 | 387 |
| 0.000 TO 0.010 | 0.010 | 365 |
| 0.010 TO 0.020 | 0.020 | 435 |
| 0.020 TO 0.030 | 0.030 | 384 |
| 0.030 TO 0.040 | 0.040 | 351 |
| 0.040 TO 0.050 | 0.050 | 322 |
| 0.050 TO 0.060 | 0.060 | 297 |
| 0.060 TO 0.070 | 0.070 | 223 |
| 0.070 TO 0.080 | 0.080 | 119 |
| 0.080 TO 0.090 | 0.090 | 0 |
| 0.090 TO 0.100 | 0.100 | 0 |
| 0.100 TO 0.110 | 0.110 | 0 |
| 0.110 TO 0.120 | 0.120 | 0 |
| 0.120 TO 0.130 | 0.130 | 0 |
| 0.130 TO 0.140 | 0.140 | 7 |
| 0.140 TO 0.150 | 0.150 | 0 |
| 0.150 TO 0.160 | 0.160 | 0 |
| 0.160 TO 0.170 | 0.170 | 0 |
| 0.170 TO 0.180 | 0.180 | 0 |
| 0.180 TO 0.190 | 0.190 | 0 |
| 0.190 TO 0.200 | 0.200 | 2 |
| GREATER THAN | 0.200 | 0 |

NO 2 OF X IN CM 1241.139 FT FROM THE TARGET

Figure 4. Beam profiles at the second focus in the vertical and horizontal planes respectively. No sextupoles are included and the momentum is the central design value.

THE FOLLOWING IS A HISTOGRAM OF X FOR 5000 RAYS

-17-

(3)
TM-374
2254.000

INTERVAL

SCALE FACTOR: 100 X'S EQUAL 436 RAYS

LESS THAN -0.222 0

| | |
|-------------------|---|
| -0.222 TO -0.190 | 0 |
| -0.190 TO -0.162 | 0 |
| -0.162 TO -0.132 | 0 |
| -0.132 TO -0.102 | 0 |
| -0.102 TO -0.072 | 0 |
| -0.072 TO -0.042 | 0 |
| -0.042 TO -0.012 | 0 |
| -0.012 TO 0.012 | 0 |
| 0.012 TO 0.042 | 0 |
| 0.042 TO 0.072 | 0 |
| 0.072 TO 0.102 | 0 |
| 0.102 TO 0.132 | 0 |
| 0.132 TO 0.162 | 0 |
| 0.162 TO 0.190 | 0 |
| 0.190 TO 0.222 | 0 |
| GREATERTHAN 0.222 | 0 |

NO 3 OF X IN CM 1470.000 FT FROM THE TARGET

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5000 RAYS

(4)

INTERVAL

SCALE FACTOR: 100 Y'S EQUAL 501 RAYS

LESS THAN -0.220 0

| | |
|-------------------|---|
| -0.220 TO -0.190 | 0 |
| -0.190 TO -0.162 | 0 |
| -0.162 TO -0.132 | 0 |
| -0.132 TO -0.102 | 0 |
| -0.102 TO -0.072 | 0 |
| -0.072 TO -0.042 | 0 |
| -0.042 TO -0.012 | 0 |
| -0.012 TO 0.012 | 0 |
| 0.012 TO 0.042 | 0 |
| 0.042 TO 0.072 | 0 |
| 0.072 TO 0.102 | 0 |
| 0.102 TO 0.132 | 0 |
| 0.132 TO 0.162 | 0 |
| 0.162 TO 0.190 | 0 |
| 0.190 TO 0.220 | 0 |
| GREATERTHAN 0.220 | 0 |

NO 4 OF Y IN CM 1470.000 FT FROM THE TARGET

Figure 5. Beam profiles at the third focus in the horizontal and vertical planes respectively. No sextupoles are included and the momentum is the central design value.

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5000 RAYS

no sexts - off + .5% (5)

-18-

TM-374
2254.000

INTERVAL SCALE FACTOR: 100 X'S EQUAL 294 RAYS

| LESS THAN | INTERVAL | N |
|--------------|----------|-----|
| -0.200 | -0.190 | 0 |
| -0.190 | -0.180 | 3 |
| -0.180 | -0.170 | 4 |
| -0.170 | -0.160 | 14 |
| -0.160 | -0.150 | 19 |
| -0.150 | -0.140 | 31 |
| -0.140 | -0.130 | 68 |
| -0.130 | -0.120 | 69 |
| -0.120 | -0.110 | 94 |
| -0.110 | -0.100 | 114 |
| -0.100 | -0.090 | 149 |
| -0.090 | -0.080 | 148 |
| -0.080 | -0.070 | 164 |
| -0.070 | -0.060 | 162 |
| -0.060 | -0.050 | 176 |
| -0.050 | -0.040 | 227 |
| -0.040 | -0.030 | 259 |
| -0.030 | -0.020 | 264 |
| -0.020 | -0.010 | 261 |
| -0.010 | 0.000 | 294 |
| 0.000 | 0.010 | 265 |
| 0.010 | 0.020 | 249 |
| 0.020 | 0.030 | 256 |
| 0.030 | 0.040 | 256 |
| 0.040 | 0.050 | 242 |
| 0.050 | 0.060 | 218 |
| 0.060 | 0.070 | 182 |
| 0.070 | 0.080 | 147 |
| 0.080 | 0.090 | 145 |
| 0.090 | 0.100 | 135 |
| 0.100 | 0.110 | 126 |
| 0.110 | 0.120 | 87 |
| 0.120 | 0.130 | 56 |
| 0.130 | 0.140 | 57 |
| 0.140 | 0.150 | 42 |
| 0.150 | 0.160 | 22 |
| 0.160 | 0.170 | 18 |
| 0.170 | 0.180 | 8 |
| 0.180 | 0.190 | 1 |
| 0.190 | 0.200 | 0 |
| GREATER THAN | 0.200 | 0 |

NO 1 OF Y IN CM 1027.139 FT FROM THE TARGET

THE FOLLOWING IS A HISTOGRAM OF X FOR 5000 RAYS

(6)

| INTERVAL | SCALE FACTOR: 100 X'S EQUAL 233 RAYS | | |
|--------------|--------------------------------------|-----|----------------------|
| LESS THAN | -2.400 | | |
| -2.400 | -2.390 | 19 | XXXX |
| -2.390 | -2.380 | 15 | XXXXXX |
| -2.380 | -2.370 | 26 | XXXXXXXXXXXX |
| -2.370 | -2.360 | 37 | XXXXXXXXXXXXXXX |
| -2.360 | -2.350 | 43 | XXXXXXXXXXXXXX |
| -2.350 | -2.340 | 55 | XXXXXXXXXXXXXX |
| -2.340 | -2.330 | 60 | XXXXXXXXXXXXXXXXXXXX |
| -2.330 | -2.320 | 99 | XXXXXXXXXXXXXXXXXXXX |
| -2.320 | -2.310 | 120 | XXXXXXXXXXXXXXXXXXXX |
| -2.310 | -2.300 | 98 | XXXXXXXXXXXXXXXXXXXX |
| -2.300 | -2.290 | 134 | XXXXXXXXXXXXXXXXXXXX |
| -2.290 | -2.280 | 175 | XXXXXXXXXXXXXXXXXXXX |
| -2.280 | -2.270 | 152 | XXXXXXXXXXXXXXXXXXXX |
| -2.270 | -2.260 | 189 | XXXXXXXXXXXXXXXXXXXX |
| -2.260 | -2.250 | 165 | XXXXXXXXXXXXXXXXXXXX |
| -2.250 | -2.240 | 175 | XXXXXXXXXXXXXXXXXXXX |
| -2.240 | -2.230 | 171 | XXXXXXXXXXXXXXXXXXXX |
| -2.230 | -2.220 | 169 | XXXXXXXXXXXXXXXXXXXX |
| -2.220 | -2.210 | 228 | XXXXXXXXXXXXXXXXXXXX |
| -2.210 | -2.200 | 233 | XXXXXXXXXXXXXXXXXXXX |
| -2.200 | -2.190 | 227 | XXXXXXXXXXXXXXXXXXXX |
| -2.190 | -2.180 | 221 | XXXXXXXXXXXXXXXXXXXX |
| -2.180 | -2.170 | 229 | XXXXXXXXXXXXXXXXXXXX |
| -2.170 | -2.160 | 268 | XXXXXXXXXXXXXXXXXXXX |
| -2.160 | -2.150 | 220 | XXXXXXXXXXXXXXXXXXXX |
| -2.150 | -2.140 | 159 | XXXXXXXXXXXXXXXXXXXX |
| -2.140 | -2.130 | 179 | XXXXXXXXXXXXXXXXXXXX |
| -2.130 | -2.120 | 163 | XXXXXXXXXXXXXXXXXXXX |
| -2.120 | -2.110 | 166 | XXXXXXXXXXXXXXXXXXXX |
| -2.110 | -2.100 | 143 | XXXXXXXXXXXXXXXXXXXX |
| -2.100 | -2.090 | 159 | XXXXXXXXXXXXXXXXXXXX |
| -2.090 | -2.080 | 111 | XXXXXXXXXXXXXXXXXXXX |
| -2.080 | -2.070 | 151 | XXXXXXXXXXXXXXXXXXXX |
| -2.070 | -2.060 | 77 | XXXXXXXXXXXXXXXXXXXX |
| -2.060 | -2.050 | 71 | XXXXXXXXXXXXXXXXXXXX |
| -2.050 | -2.040 | 65 | XXXXXXXXXXXXXXXXXXXX |
| -2.040 | -2.030 | 49 | XXXXXXXXXXXXXXXXXXXX |
| -2.030 | -2.020 | 33 | XXXXXX |
| -2.020 | -2.010 | 19 | XXXXXX |
| -2.010 | -2.000 | 15 | XXXXXX |
| GREATER THAN | -2.000 | | |
| | 11 XXXX | | |

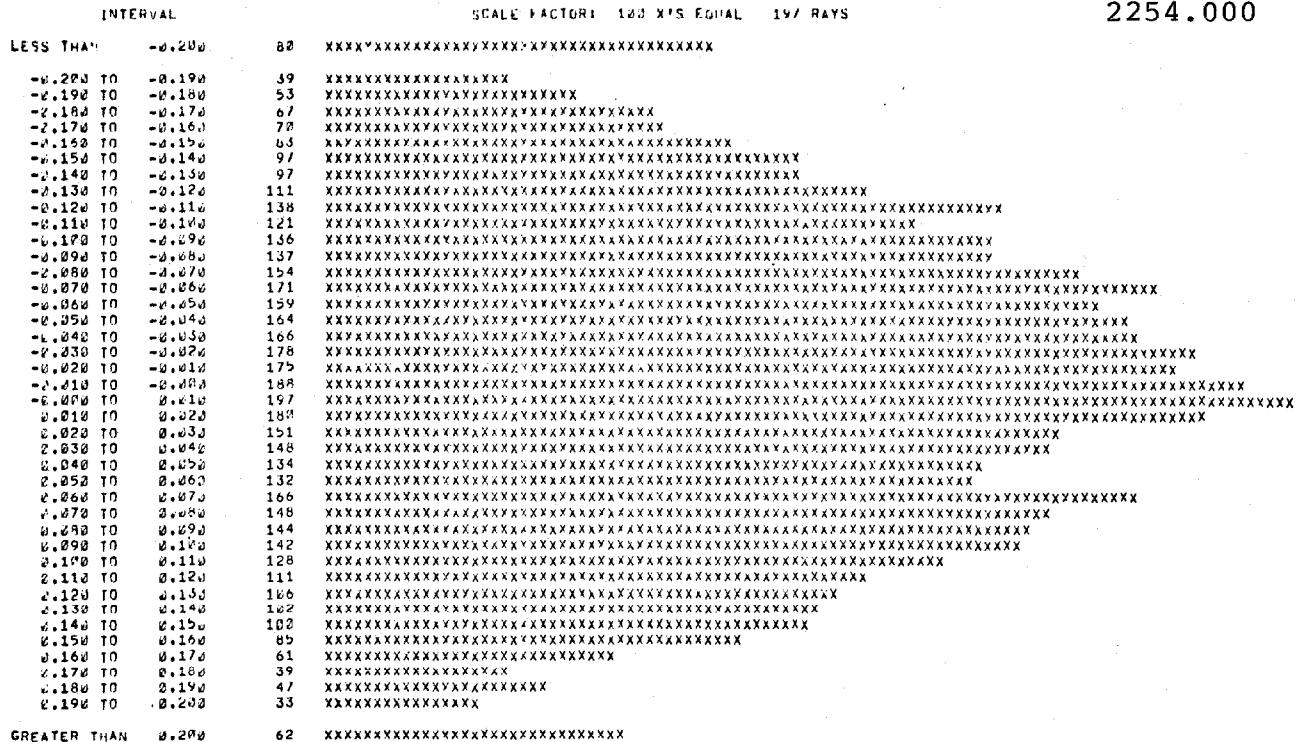
NO 2 OF X IN CM 1041.139 FT FROM THE TARGET

Figure 6. Beam profiles at the second focus in the vertical and horizontal planes respectively. No sextupoles are included and the momentum is one-half percent above the central design value.

THE FOLLOWING IS A HISTOGRAM OF X FOR 5000 RAYS

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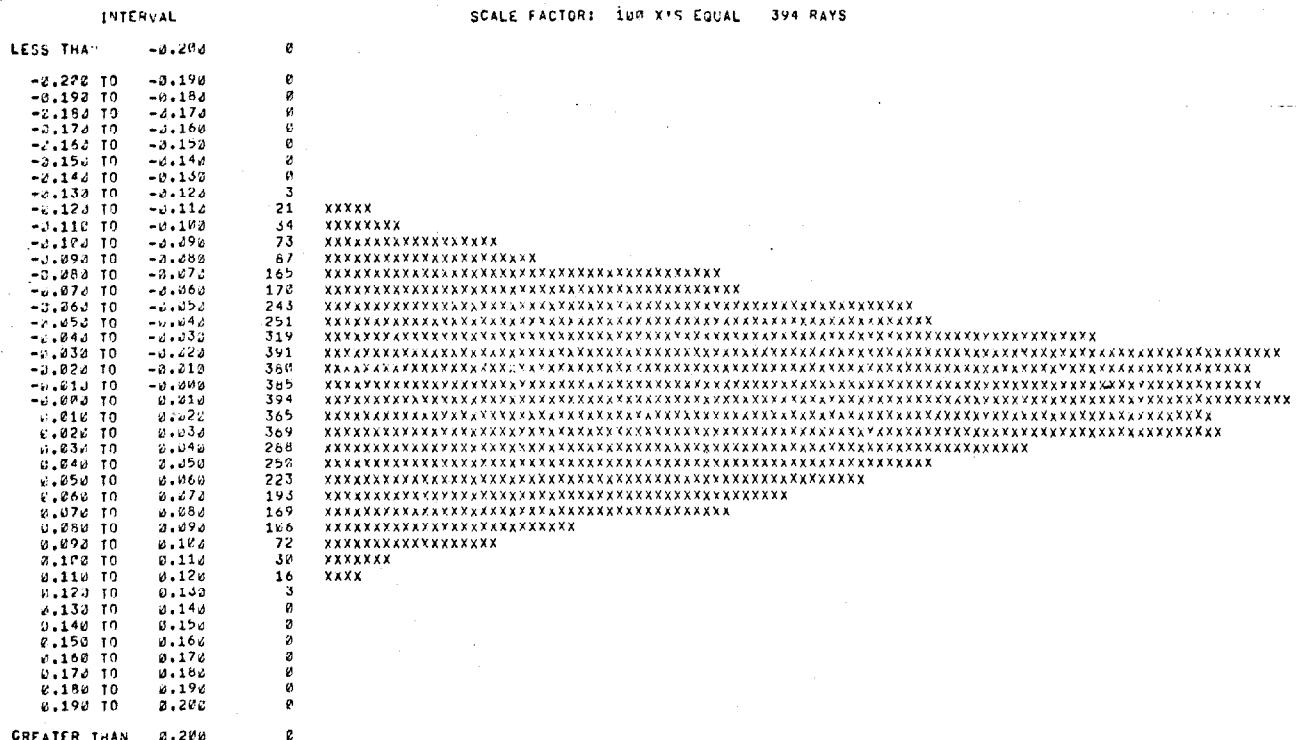
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NO 3 OF X IN CM 1473.000 FT FROM THE TARGET

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5000 RAYS

(8)



NO 4 OF Y IN CM 1470.000 FT FROM THE TARGET

Figure 7. Beam profiles at the third focus in the horizontal and vertical planes respectively. No sextupoles are included and the momentum is one-half percent above the central design value.

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5800 RAYS

No sexts. $\Delta p/p = 1\%$ (a)

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| INTERVAL | | SCALE FACTOR: 122 X'S EQUAL 188 RAYS |
|-------------|--------|---|
| LESS THAN | -0.2°0 | 82 XXXXXXXX'XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.190 | 47 XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.180 | 50 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.170 | 63 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.160 | 77 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.150 | 98 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.140 | 86 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.130 | 81 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.120 | 115 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.110 | 116 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.100 | 122 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.090 | 114 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.080 | 153 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.070 | 152 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.060 | 134 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.050 | 177 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.040 | 152 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.030 | 158 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | -0.020 | 167 XXXXXXXX XXXXXXXXXXXXXXXXX |
| | -0.010 | 164 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.000 | 188 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.010 | 144 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.020 | 172 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.030 | 158 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.040 | 168 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.050 | 151 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.060 | 152 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.070 | 153 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.080 | 147 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.090 | 148 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.100 | 131 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.110 | 114 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.120 | 101 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.130 | 88 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.140 | 97 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.150 | 74 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.160 | 82 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.170 | 66 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.180 | 34 XXXXXXXXXXXXXXXXXXXXXXXXX |
| | 0.190 | 43 XXXXXXXXXXXXXXXXXXXXXXXXX |
| GREATERTHAN | 0.200 | 123 XXX |

NO 1 OF Y IN CM 1027.139 FT FROM THE TARGET

THE FOLLOWING IS A HISTOGRAM OF X FOR 5800 RAYS

| INTERVAL | | SCALE FACTOR: 122 X'S EQUAL 766 RAYS |
|-------------|--------|---|
| LESS THAN | -4.620 | 351 XXXXXXXX'XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| | -4.590 | 77 XXXXXXXXXX |
| | -4.560 | 73 XXXXXXXXXX |
| | -4.530 | 68 XXXXXXXXXX |
| | -4.500 | 77 XXXXXXXXXX |
| | -4.480 | 95 XXXXXXXXXX |
| | -4.460 | 77 XXXXXXXXXX |
| | -4.440 | 93 XXXXXXXXXX |
| | -4.420 | 99 XXXXXXXXXX |
| | -4.400 | 99 XXXXXXXXXX |
| | -4.380 | 87 XXXXXXXXXX |
| | -4.360 | 89 XXXXXXXXXX |
| | -4.340 | 90 XXXXXXXXXX |
| | -4.320 | 95 XXXXXXXXXX |
| | -4.300 | 102 XXXXXXXXXX |
| | -4.280 | 87 XXXXXXXXXX |
| | -4.260 | 111 XXXXXXXXXX |
| | -4.240 | 108 XXXXXXXXXX |
| | -4.220 | 92 YXXXXXXX |
| | -4.200 | 131 XXXXXXXXXX |
| | -4.180 | 97 XXXXXXXXXX |
| | -4.160 | 114 XXXXXXXXXX |
| | -4.140 | 118 XXXXXXXXXX |
| | -4.120 | 116 XXXXXXXXXX |
| | -4.100 | 122 XXXXXXXXXX |
| | -4.080 | 114 XXXXXXXXXX |
| | -4.060 | 114 XXXXXXXXXX |
| | -4.040 | 124 XXXXXXXXXX |
| | -4.020 | 132 XXXXXXXXXX |
| | -4.000 | 127 XXXXXXXXXX |
| | -3.980 | 129 XXXXXXXXXX |
| | -3.960 | 103 XXXXXXXXXX |
| | -3.940 | 114 XXXXXXXXXX |
| | -3.920 | 120 XXXXXXXXXX |
| | -3.900 | 97 XXXXXXXXXX |
| | -3.880 | 99 XXXXXXXXXX |
| | -3.860 | 96 XXXXXXXXXX |
| | -3.840 | 84 XXXXXXXXXX |
| | -3.820 | 77 XXXXXXXXXX |
| | -3.800 | 101 XXXXXXXXXX |
| | -3.780 | 96 XXXXXXXXXX |
| | -3.760 | 80 XXXXXXXXXX |
| GREATERTHAN | 0.200 | 766 XXX |

NO 2 OF X IN CM 1041.139 FT FROM THE TARGET

Figure 8. Beam profiles at the second focus in the vertical and horizontal planes respectively. No sextupoles are included and the momentum is one percent above the central design value.

THE FOLLOWING IS A HISTOGRAM OF X FOR 5000 RAYS

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| INTERVAL | SCALE FACTOR: 100 X'S EQUAL 1032 RAYS |
|-------------------|--|
| LESS THAN -0.200 | 1032 XXX |
| -0.190 TO -0.190 | 73 XXXXXXXX |
| -0.180 TO -0.170 | 64 XXXXXXXX |
| -0.170 TO -0.160 | 67 XXXXXXXX |
| -0.160 TO -0.150 | 86 XXXXXXXX |
| -0.150 TO -0.140 | 73 XXXXXXXX |
| -0.140 TO -0.130 | 78 XXXXXXXX |
| -0.130 TO -0.120 | 78 XXXXXXXX |
| -0.120 TO -0.110 | 82 XXXXXXXX |
| -0.110 TO -0.100 | 84 XXXXXXXX |
| -0.100 TO -0.090 | 93 XXXXXXXXXX |
| -0.090 TO -0.080 | 94 XXXXXXXXXX |
| -0.080 TO -0.070 | 102 XXXXXXXXXX |
| -0.070 TO -0.060 | 94 XXXXXXXXXX |
| -0.060 TO -0.050 | 75 XXXXXXXX |
| -0.050 TO -0.040 | 101 XXXXXXXXXX |
| -0.040 TO -0.030 | 81 XXXXXXXX |
| -0.030 TO -0.020 | 88 XXXXXXXX |
| -0.020 TO -0.010 | 99 XXXXXXXX |
| -0.010 TO 0.000 | 90 XXXXXXXX |
| 0.000 TO 0.010 | 91 XXXXXXXX |
| 0.010 TO 0.020 | 83 XXXXXXXX |
| 0.020 TO 0.030 | 76 XXXXXXXX |
| 0.030 TO 0.040 | 51 XXXXXXXX |
| 0.040 TO 0.050 | 79 XXXXXXXX |
| 0.050 TO 0.060 | 63 XXXXXXXX |
| 0.060 TO 0.070 | 96 XXXXXXXXXX |
| 0.070 TO 0.080 | 91 XXXXXXXX |
| 0.080 TO 0.090 | 81 XXXXXXXX |
| 0.090 TO 0.100 | 82 XXXXXXXX |
| 0.100 TO 0.110 | 82 XXXXXXXX |
| 0.110 TO 0.120 | 65 XXXXXXXX |
| 0.120 TO 0.130 | 80 XXXXXXXX |
| 0.130 TO 0.140 | 59 XXXXXXXX |
| 0.140 TO 0.150 | 78 XXXXXXXX |
| 0.150 TO 0.160 | 59 XXXXXXXX |
| 0.160 TO 0.170 | 93 XXXXXXXXXX |
| 0.170 TO 0.180 | 75 XXXXXXXX |
| 0.180 TO 0.190 | 60 XXXXXXXX |
| 0.190 TO 0.200 | 74 XXXXXXXX |
| GREATERTHAN 0.200 | 726 XXX |

NO 3 OF X IN CM 1472.020 FT FROM THE TARGET

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5000 RAYS

(12)

| INTERVAL | SCALE FACTOR: 100 Y'S EQUAL 237 RAYS |
|-------------------|--------------------------------------|
| LESS THAN -0.200 | 0 |
| -0.190 TO -0.190 | 0 |
| -0.180 TO -0.180 | 2 |
| -0.180 TO -0.170 | 14 XXXXX |
| -0.170 TO -0.150 | 22 XXXXXXXX |
| -0.160 TO -0.150 | 34 XXXXXXXXXX |
| -0.150 TO -0.140 | 51 XXXXXXXXXXXXXXXXXX |
| -0.140 TO -0.130 | 63 XXXXXXXXXXXXXXXXXX |
| -0.130 TO -0.120 | 96 XXXXXXXXXXXXXXXXXX |
| -0.120 TO -0.110 | 118 XXXXXXXXXXXXXXXXXX |
| -0.110 TO -0.100 | 124 XXXXXXXXXXXXXXXXXX |
| -0.100 TO -0.090 | 134 XXXXXXXXXXXXXXXXXX |
| -0.090 TO -0.080 | 162 XXXXXXXXXXXXXXXXXX |
| -0.080 TO -0.070 | 21' XXXXXXXXXXXXXXXXXX |
| -0.070 TO -0.060 | 193 XXXXXXXXXXXXXXXXXX |
| -0.060 TO -0.050 | 225 XXXXXXXXXXXXXXXXXX |
| -0.050 TO -0.040 | 22' XXXXXXXXXXXXXXXXXX |
| -0.040 TO -0.030 | 224 XXXXXXXXXXXXXXXXXX |
| -0.030 TO -0.020 | 231 XXXXXXXXXXXXXXXXXX |
| -0.020 TO -0.010 | 237 XXXXXXXXXXXXXXXXXX |
| -0.010 TO 0.000 | 224 XXXXXXXXXXXXXXXXXX |
| 0.000 TO 0.010 | 221 XXXXXXXXXXXXXXXXXX |
| 0.010 TO 0.020 | 211 XXXXXXXXXXXXXXXXXX |
| 0.020 TO 0.030 | 214 XXXXXXXXXXXXXXXXXX |
| 0.030 TO 0.040 | 214 XXXXXXXXXXXXXXXXXX |
| 0.040 TO 0.050 | 215 XXXXXXXXXXXXXXXXXX |
| 0.050 TO 0.060 | 194 XXXXXXXXXXXXXXXXXX |
| 0.060 TO 0.070 | 172 XXXXXXXXXXXXXXXXXX |
| 0.070 TO 0.080 | 182 XXXXXXXXXXXXXXXXXX |
| 0.080 TO 0.090 | 164 XXXXXXXXXXXXXXXXXX |
| 0.090 TO 0.100 | 143 XXXXXXXXXXXXXXXXXX |
| 0.100 TO 0.110 | 13' XXXXXXXXXXXXXXXXXX |
| 0.110 TO 0.120 | 121 XXXXXXXXXXXXXXXXXX |
| 0.120 TO 0.130 | 128 XXXXXXXXXXXXXXXXXX |
| 0.130 TO 0.140 | 61 XXXXXXXXXXXXXXXXXX |
| 0.140 TO 0.150 | 57 XXXXXXXXXXXXXXXXXX |
| 0.150 TO 0.160 | 22 XXXXXXXXXX |
| 0.160 TO 0.170 | 22 XXXXXXXXXX |
| 0.170 TO 0.180 | 6 XX |
| 0.180 TO 0.190 | 2 XX |
| 0.190 TO 0.200 | 0 |
| GREATERTHAN 0.200 | 0 |

NO 4 OF Y IN CM 1472.020 FT FROM THE TARGET

Figure 9. Beam profiles at the third focus in the horizontal and vertical planes respectively. No sextupoles are included and the momentum is one percent above the central design value.

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5000 RAYS

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2 sexts - Δ/p = 0 (13)

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2254.000

INTERVAL

SCALE FACTOR: 100 X'S EQUAL 318 RAYS

| LESS THAN | INTERVAL | COUNT |
|--------------|-----------|-------|
| | -2.200 | 0 |
| -2.272 | TO -2.192 | 0 |
| -2.192 | TO -2.180 | 2 |
| -2.180 | TO -2.170 | 2 |
| -2.170 | TO -2.160 | 0 |
| -2.160 | TO -2.150 | 0 |
| -2.150 | TO -2.142 | 0 |
| -2.142 | TO -2.132 | 2 |
| -2.132 | TO -2.122 | 0 |
| -2.122 | TO -2.110 | 5 |
| -2.110 | TO -2.100 | 54 |
| -2.100 | TO -2.070 | 123 |
| -2.070 | TO -2.040 | 170 |
| -2.040 | TO -2.020 | 234 |
| -2.020 | TO -2.000 | 261 |
| -2.000 | TO -2.000 | 234 |
| -2.000 | TO -2.000 | 245 |
| -2.000 | TO -2.000 | 29 |
| -2.000 | TO -2.000 | 295 |
| -2.000 | TO -2.000 | 299 |
| -2.000 | TO -2.000 | 303 |
| -2.000 | TO -2.000 | 275 |
| -2.000 | TO -2.000 | 318 |
| -2.000 | TO -2.000 | 312 |
| -2.000 | TO -2.000 | 332 |
| -2.000 | TO -2.000 | 247 |
| -2.000 | TO -2.000 | 243 |
| -2.000 | TO -2.000 | 225 |
| -2.000 | TO -2.000 | 211 |
| -2.000 | TO -2.000 | 177 |
| -2.000 | TO -2.000 | 112 |
| -2.000 | TO -2.000 | 61 |
| -2.000 | TO -2.000 | 2 |
| -2.000 | TO -2.000 | 0 |
| GREATER THAN | 0.200 | 0 |

NO 1 OF Y IN CM 1027.139 FT FROM THE TARGET

(14)

THE FOLLOWING IS A HISTOGRAM OF X FOR 5000 RAYS

| INTERVAL | SCALE FACTOR: 100 X'S EQUAL 400 RAYS | |
|--------------|--------------------------------------|-----|
| LESS THAN | -2.272 | |
| -2.272 | TO -2.192 | 0 |
| -2.192 | TO -2.180 | 2 |
| -2.180 | TO -2.170 | 2 |
| -2.170 | TO -2.160 | 0 |
| -2.160 | TO -2.150 | 0 |
| -2.150 | TO -2.142 | 0 |
| -2.142 | TO -2.132 | 0 |
| -2.132 | TO -2.122 | 4 |
| -2.122 | TO -2.112 | 7 |
| -2.112 | TO -2.110 | 12 |
| -2.110 | TO -2.110 | 3 |
| -2.110 | TO -2.090 | 28 |
| -2.090 | TO -2.070 | 64 |
| -2.070 | TO -2.070 | 112 |
| -2.070 | TO -2.050 | 199 |
| -2.050 | TO -2.050 | 225 |
| -2.050 | TO -2.042 | 304 |
| -2.042 | TO -2.030 | 337 |
| -2.030 | TO -2.020 | 363 |
| -2.020 | TO -2.010 | 427 |
| -2.010 | TO -2.000 | 386 |
| -2.000 | TO -2.010 | 357 |
| -2.010 | TO -2.000 | 396 |
| -2.000 | TO -2.000 | 374 |
| -2.000 | TO -2.000 | 369 |
| -2.000 | TO -2.000 | 328 |
| -2.000 | TO -2.000 | 262 |
| -2.000 | TO -2.000 | 227 |
| -2.000 | TO -2.000 | 139 |
| -2.000 | TO -2.000 | 46 |
| -2.000 | TO -2.000 | 24 |
| -2.000 | TO -2.000 | 10 |
| -2.000 | TO -2.000 | 3 |
| -2.000 | TO -2.000 | 0 |
| GREATER THAN | 0.200 | |

NO 2 OF X IN CM 1041.139 FT FROM THE TARGET

Figure 10. Beam profiles at the second focus in the vertical and horizontal planes respectively. Two sextupoles are used and the momentum is the central design value.

THE FOLLOWING IS A HISTOGRAM OF X FOR 5000 RAYS

-23-

(15)
TM-374
2254.000

INTERVAL

SCALE FACTOR: 100 X IS EQUAL 398 RAYS

| LESS THAN | INTERVAL | COUNT |
|--------------|------------------|-------|
| | -0.200 TO -0.190 | 0 |
| | -0.190 TO -0.180 | 0 |
| | -0.180 TO -0.170 | 0 |
| | -0.170 TO -0.160 | 0 |
| | -0.160 TO -0.150 | 0 |
| | -0.150 TO -0.140 | 0 |
| | -0.140 TO -0.130 | 0 |
| | -0.130 TO -0.120 | 0 |
| | -0.120 TO -0.110 | 0 |
| | -0.110 TO -0.100 | 19 |
| | -0.100 TO -0.090 | 24 |
| | -0.090 TO -0.080 | 46 |
| | -0.080 TO -0.070 | 144 |
| | -0.070 TO -0.060 | 225 |
| | -0.060 TO -0.050 | 262 |
| | -0.050 TO -0.040 | 324 |
| | -0.040 TO -0.030 | 369 |
| | -0.030 TO -0.020 | 377 |
| | -0.020 TO -0.010 | 397 |
| | -0.010 TO 0.000 | 349 |
| | 0.000 TO 0.010 | 391 |
| | 0.010 TO 0.020 | 391 |
| | 0.020 TO 0.030 | 362 |
| | 0.030 TO 0.040 | 335 |
| | 0.040 TO 0.050 | 373 |
| | 0.050 TO 0.060 | 224 |
| | 0.060 TO 0.070 | 202 |
| | 0.070 TO 0.080 | 114 |
| | 0.080 TO 0.090 | 63 |
| | 0.090 TO 0.100 | 31 |
| | 0.100 TO 0.110 | 13 |
| | 0.110 TO 0.120 | 6 |
| | 0.120 TO 0.130 | 5 |
| | 0.130 TO 0.140 | 0 |
| | 0.140 TO 0.150 | 0 |
| | 0.150 TO 0.160 | 0 |
| | 0.160 TO 0.170 | 0 |
| | 0.170 TO 0.180 | 0 |
| | 0.180 TO 0.190 | 0 |
| | 0.190 TO 0.200 | 0 |
| GREATER THAN | 0.200 | 0 |

NO 3 OF X IN CM 1472.000 FT FROM THE TARGET

(16)

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5000 RAYS

INTERVAL

SCALE FACTOR: 100 Y IS EQUAL 498 RAYS

| LESS THAN | INTERVAL | COUNT |
|--------------|------------------|-------|
| | -0.200 TO -0.190 | 0 |
| | -0.190 TO -0.180 | 0 |
| | -0.180 TO -0.170 | 0 |
| | -0.170 TO -0.160 | 0 |
| | -0.160 TO -0.150 | 0 |
| | -0.150 TO -0.140 | 0 |
| | -0.140 TO -0.130 | 0 |
| | -0.130 TO -0.120 | 0 |
| | -0.120 TO -0.110 | 0 |
| | -0.110 TO -0.100 | 0 |
| | -0.100 TO -0.090 | 0 |
| | -0.090 TO -0.080 | 0 |
| | -0.080 TO -0.070 | 0 |
| | -0.070 TO -0.060 | 98 |
| | -0.060 TO -0.050 | 245 |
| | -0.050 TO -0.040 | 346 |
| | -0.040 TO -0.030 | 384 |
| | -0.030 TO -0.020 | 447 |
| | -0.020 TO -0.010 | 493 |
| | -0.010 TO 0.000 | 467 |
| | 0.000 TO 0.010 | 478 |
| | 0.010 TO 0.020 | 491 |
| | 0.020 TO 0.030 | 424 |
| | 0.030 TO 0.040 | 472 |
| | 0.040 TO 0.050 | 381 |
| | 0.050 TO 0.060 | 252 |
| | 0.060 TO 0.070 | 85 |
| | 0.070 TO 0.080 | 2 |
| | 0.080 TO 0.090 | 0 |
| | 0.090 TO 0.100 | 0 |
| | 0.100 TO 0.110 | 0 |
| | 0.110 TO 0.120 | 0 |
| | 0.120 TO 0.130 | 0 |
| | 0.130 TO 0.140 | 0 |
| | 0.140 TO 0.150 | 0 |
| | 0.150 TO 0.160 | 0 |
| | 0.160 TO 0.170 | 0 |
| | 0.170 TO 0.180 | 0 |
| | 0.180 TO 0.190 | 0 |
| | 0.190 TO 0.200 | 0 |
| GREATER THAN | 0.200 | 0 |

NO 4 OF Y IN CM 1472.000 FT FROM THE TARGET

Figure 11. Beam profiles at the third focus in the horizontal and vertical planes respectively. Two sextupoles are used and the momentum is the central design value.

INTERVAL

SCALE FACTOR: 100 X'S EQUAL 238 RAYS

LESS THAN -0.240 3

| | | |
|------------------|-----|--------------|
| -0.220 TO -0.190 | 9 | XXX |
| -0.190 TO -0.180 | 14 | XXXXX |
| -0.180 TO -0.170 | 20 | XXXXXX |
| -0.170 TO -0.160 | 29 | XXXXXXX |
| -0.160 TO -0.150 | 53 | XXXXXXXX |
| -0.150 TO -0.140 | 53 | XXXXXXXX |
| -0.140 TO -0.130 | 94 | XXXXXXXXX |
| -0.130 TO -0.120 | 92 | XXXXXXXXX |
| -0.120 TO -0.110 | 112 | XXXXXXXXXXXX |
| -0.110 TO -0.100 | 115 | XXXXXXXXXXXX |
| -0.100 TO -0.090 | 123 | XXXXXXXXXXXX |
| -0.090 TO -0.080 | 142 | XXXXXXXXXXXX |
| -0.080 TO -0.070 | 158 | XXXXXXXXXXXX |
| -0.070 TO -0.060 | 17 | XXXXXXXXXXXX |
| -0.060 TO -0.050 | 183 | XXXXXXXXXXXX |
| -0.050 TO -0.040 | 198 | XXXXXXXXXXXX |
| -0.040 TO -0.030 | 228 | XXXXXXXXXXXX |
| -0.030 TO -0.020 | 238 | XXXXXXXXXXXX |
| -0.020 TO -0.010 | 213 | XXXXXXXXXXXX |
| -0.010 TO -0.000 | 238 | XXXXXXXXXXXX |
| 0.000 TO 0.010 | 219 | XXXXXXXXXXXX |
| 0.010 TO 0.020 | 235 | XXXXXXXXXXXX |
| 0.020 TO 0.030 | 231 | XXXXXXXXXXXX |
| 0.030 TO 0.040 | 221 | XXXXXXXXXXXX |
| 0.040 TO 0.050 | 227 | XXXXXXXXXXXX |
| 0.050 TO 0.060 | 211 | XXXXXXXXXXXX |
| 0.060 TO 0.070 | 183 | XXXXXXXXXXXX |
| 0.070 TO 0.080 | 139 | XXXXXXXXXXXX |
| 0.080 TO 0.090 | 144 | XXXXXXXXXXXX |
| 0.090 TO 0.100 | 166 | XXXXXXXXXXXX |
| 0.100 TO 0.110 | 93 | XXXXXXXXXXXX |
| 0.110 TO 0.120 | 97 | XXXXXXXXXXXX |
| 0.120 TO 0.130 | 93 | XXXXXXXXXXXX |
| 0.130 TO 0.140 | 85 | XXXXXXXXXXXX |
| 0.140 TO 0.150 | 46 | XXXXXXXXXXXX |
| 0.150 TO 0.160 | 47 | XXXXXXXXXXXX |
| 0.160 TO 0.170 | 38 | XXXXXXXXXXXX |
| 0.170 TO 0.180 | 19 | XXXXXX |
| 0.180 TO 0.190 | 13 | XXXXX |
| 0.190 TO 0.200 | 14 | XXXXX |

GREATER THAN 0.200 5 XX

NO 1 OF Y IN CM 1027.139 FT FROM THE TARGET

(18)

THE FOLLOWING IS A HISTOGRAM OF X FOR 5000 RAYS

SCALE FACTOR: 100 X'S EQUAL 395 RAYS

INTERVAL

| | | |
|------------------|-----|--------------|
| LESS THAN -2.470 | 0 | |
| -2.420 TO -2.390 | 2 | |
| -2.390 TO -2.380 | 0 | |
| -2.380 TO -2.370 | 0 | |
| -2.370 TO -2.342 | 0 | |
| -2.342 TO -2.350 | 0 | |
| -2.352 TO -2.340 | 0 | |
| -2.340 TO -2.330 | 1 | |
| -2.330 TO -2.320 | 7 | X |
| -2.320 TO -2.310 | 7 | X |
| -2.310 TO -2.300 | 17 | XXXX |
| -2.300 TO -2.290 | 33 | XXXXXX |
| -2.290 TO -2.280 | 92 | XXXXXXXX |
| -2.280 TO -2.270 | 151 | XXXXXXXXXXXX |
| -2.270 TO -2.260 | 21 | XXXXXXXXXXXX |
| -2.260 TO -2.250 | 254 | XXXXXXXXXXXX |
| -2.250 TO -2.240 | 331 | XXXXXXXXXXXX |
| -2.240 TO -2.230 | 356 | XXXXXXXXXXXX |
| -2.230 TO -2.220 | 394 | XXXXXXXXXXXX |
| -2.220 TO -2.210 | 394 | XXXXXXXXXXXX |
| -2.210 TO -2.200 | 371 | XXXXXXXXXXXX |
| -2.200 TO -2.190 | 397 | XXXXXXXXXXXX |
| -2.190 TO -2.180 | 367 | XXXXXXXXXXXX |
| -2.180 TO -2.170 | 395 | XXXXXXXXXXXX |
| -2.170 TO -2.160 | 344 | XXXXXXXXXXXX |
| -2.160 TO -2.150 | 292 | XXXXXXXXXXXX |
| -2.150 TO -2.140 | 267 | XXXXXXXXXXXX |
| -2.140 TO -2.130 | 195 | XXXXXXXXXXXX |
| -2.130 TO -2.120 | 94 | XXXXXXXXXXXX |
| -2.120 TO -2.110 | 35 | XXXXXX |
| -2.110 TO -2.100 | 1 | XX |
| -2.100 TO -2.090 | 7 | X |
| -2.090 TO -2.080 | 2 | |
| -2.080 TO -2.070 | 4 | |
| -2.070 TO -2.060 | 2 | |
| -2.060 TO -2.050 | 2 | |
| -2.050 TO -2.040 | 0 | |
| -2.040 TO -2.030 | 2 | |
| -2.030 TO -2.020 | 2 | |
| -2.020 TO -2.010 | 0 | |
| -2.010 TO -2.000 | 0 | |

GREATER THAN -2.000 0

NO 2 OF X IN CM 1041.139 FT FROM THE TARGET

Figure 12. Beam profiles at the second focus in the vertical and horizontal planes respectively. Two sextupoles are used and the momentum is one-half percent above the central design value.

THE FOLLOWING IS A HISTOGRAM OF X FOR 5000 RAYS

-25-

(19)
TM-374
2254.000

| INTERVAL | SCALE FACTOR: 100 X'S EQUAL 417 RAYS |
|-------------------|--------------------------------------|
| LESS THAN -0.200 | -0.200 |
| -0.200 TO -0.198 | 0 |
| -0.198 TO -0.196 | 0 |
| -0.196 TO -0.194 | 0 |
| -0.194 TO -0.192 | 0 |
| -0.192 TO -0.190 | 0 |
| -0.190 TO -0.188 | 0 |
| -0.188 TO -0.186 | 0 |
| -0.186 TO -0.184 | 0 |
| -0.184 TO -0.182 | 0 |
| -0.182 TO -0.180 | 0 |
| -0.180 TO -0.178 | 0 |
| -0.178 TO -0.176 | 0 |
| -0.176 TO -0.174 | 0 |
| -0.174 TO -0.172 | 0 |
| -0.172 TO -0.170 | 0 |
| -0.170 TO -0.168 | 0 |
| -0.168 TO -0.166 | 0 |
| -0.166 TO -0.164 | 0 |
| -0.164 TO -0.162 | 0 |
| -0.162 TO -0.160 | 0 |
| -0.160 TO -0.158 | 0 |
| -0.158 TO -0.156 | 0 |
| -0.156 TO -0.154 | 0 |
| -0.154 TO -0.152 | 0 |
| -0.152 TO -0.150 | 0 |
| -0.150 TO -0.148 | 0 |
| -0.148 TO -0.146 | 0 |
| -0.146 TO -0.144 | 0 |
| -0.144 TO -0.142 | 0 |
| -0.142 TO -0.140 | 0 |
| -0.140 TO -0.138 | 0 |
| -0.138 TO -0.136 | 0 |
| -0.136 TO -0.134 | 0 |
| -0.134 TO -0.132 | 0 |
| -0.132 TO -0.130 | 0 |
| -0.130 TO -0.128 | 0 |
| -0.128 TO -0.126 | 0 |
| -0.126 TO -0.124 | 0 |
| -0.124 TO -0.122 | 0 |
| -0.122 TO -0.120 | 0 |
| -0.120 TO -0.118 | 0 |
| -0.118 TO -0.116 | 0 |
| -0.116 TO -0.114 | 0 |
| -0.114 TO -0.112 | 0 |
| -0.112 TO -0.110 | 0 |
| -0.110 TO -0.108 | 0 |
| -0.108 TO -0.106 | 0 |
| -0.106 TO -0.104 | 0 |
| -0.104 TO -0.102 | 0 |
| -0.102 TO -0.100 | 0 |
| -0.100 TO -0.098 | 0 |
| -0.098 TO -0.096 | 0 |
| -0.096 TO -0.094 | 0 |
| -0.094 TO -0.092 | 0 |
| -0.092 TO -0.090 | 0 |
| -0.090 TO -0.088 | 0 |
| -0.088 TO -0.086 | 0 |
| -0.086 TO -0.084 | 0 |
| -0.084 TO -0.082 | 0 |
| -0.082 TO -0.080 | 0 |
| -0.080 TO -0.078 | 0 |
| -0.078 TO -0.076 | 0 |
| -0.076 TO -0.074 | 0 |
| -0.074 TO -0.072 | 0 |
| -0.072 TO -0.070 | 0 |
| -0.070 TO -0.068 | 0 |
| -0.068 TO -0.066 | 0 |
| -0.066 TO -0.064 | 0 |
| -0.064 TO -0.062 | 0 |
| -0.062 TO -0.060 | 0 |
| -0.060 TO -0.058 | 0 |
| -0.058 TO -0.056 | 0 |
| -0.056 TO -0.054 | 0 |
| -0.054 TO -0.052 | 0 |
| -0.052 TO -0.050 | 0 |
| -0.050 TO -0.048 | 0 |
| -0.048 TO -0.046 | 0 |
| -0.046 TO -0.044 | 0 |
| -0.044 TO -0.042 | 0 |
| -0.042 TO -0.040 | 0 |
| -0.040 TO -0.038 | 0 |
| -0.038 TO -0.036 | 0 |
| -0.036 TO -0.034 | 0 |
| -0.034 TO -0.032 | 0 |
| -0.032 TO -0.030 | 0 |
| -0.030 TO -0.028 | 0 |
| -0.028 TO -0.026 | 0 |
| -0.026 TO -0.024 | 0 |
| -0.024 TO -0.022 | 0 |
| -0.022 TO -0.020 | 0 |
| -0.020 TO -0.018 | 0 |
| -0.018 TO -0.016 | 0 |
| -0.016 TO -0.014 | 0 |
| -0.014 TO -0.012 | 0 |
| -0.012 TO -0.010 | 0 |
| -0.010 TO -0.008 | 0 |
| -0.008 TO -0.006 | 0 |
| -0.006 TO -0.004 | 0 |
| -0.004 TO -0.002 | 0 |
| -0.002 TO 0.000 | 0 |
| GREATERTHAN 0.000 | 0 |

NO 3 OF X IN CM 1470.000 FT FROM THE TARGET

(20)

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5000 RAYS

| INTERVAL | SCALE FACTOR: 100 Y'S EQUAL 332 RAYS |
|-------------------|--------------------------------------|
| LESS THAN -0.200 | -0.200 |
| -0.200 TO -0.198 | 0 |
| -0.198 TO -0.196 | 0 |
| -0.196 TO -0.194 | 0 |
| -0.194 TO -0.192 | 0 |
| -0.192 TO -0.190 | 0 |
| -0.190 TO -0.188 | 0 |
| -0.188 TO -0.186 | 0 |
| -0.186 TO -0.184 | 0 |
| -0.184 TO -0.182 | 0 |
| -0.182 TO -0.180 | 0 |
| -0.180 TO -0.178 | 0 |
| -0.178 TO -0.176 | 0 |
| -0.176 TO -0.174 | 0 |
| -0.174 TO -0.172 | 0 |
| -0.172 TO -0.170 | 0 |
| -0.170 TO -0.168 | 0 |
| -0.168 TO -0.166 | 0 |
| -0.166 TO -0.164 | 0 |
| -0.164 TO -0.162 | 0 |
| -0.162 TO -0.160 | 0 |
| -0.160 TO -0.158 | 0 |
| -0.158 TO -0.156 | 0 |
| -0.156 TO -0.154 | 0 |
| -0.154 TO -0.152 | 0 |
| -0.152 TO -0.150 | 0 |
| -0.150 TO -0.148 | 0 |
| -0.148 TO -0.146 | 0 |
| -0.146 TO -0.144 | 0 |
| -0.144 TO -0.142 | 0 |
| -0.142 TO -0.140 | 0 |
| -0.140 TO -0.138 | 0 |
| -0.138 TO -0.136 | 0 |
| -0.136 TO -0.134 | 0 |
| -0.134 TO -0.132 | 0 |
| -0.132 TO -0.130 | 0 |
| -0.130 TO -0.128 | 0 |
| -0.128 TO -0.126 | 0 |
| -0.126 TO -0.124 | 0 |
| -0.124 TO -0.122 | 0 |
| -0.122 TO -0.120 | 0 |
| -0.120 TO -0.118 | 0 |
| -0.118 TO -0.116 | 0 |
| -0.116 TO -0.114 | 0 |
| -0.114 TO -0.112 | 0 |
| -0.112 TO -0.110 | 0 |
| -0.110 TO -0.108 | 0 |
| -0.108 TO -0.106 | 0 |
| -0.106 TO -0.104 | 0 |
| -0.104 TO -0.102 | 0 |
| -0.102 TO -0.100 | 0 |
| -0.100 TO -0.098 | 0 |
| -0.098 TO -0.096 | 0 |
| -0.096 TO -0.094 | 0 |
| -0.094 TO -0.092 | 0 |
| -0.092 TO -0.090 | 0 |
| -0.090 TO -0.088 | 0 |
| -0.088 TO -0.086 | 0 |
| -0.086 TO -0.084 | 0 |
| -0.084 TO -0.082 | 0 |
| -0.082 TO -0.080 | 0 |
| -0.080 TO -0.078 | 0 |
| -0.078 TO -0.076 | 0 |
| -0.076 TO -0.074 | 0 |
| -0.074 TO -0.072 | 0 |
| -0.072 TO -0.070 | 0 |
| -0.070 TO -0.068 | 0 |
| -0.068 TO -0.066 | 0 |
| -0.066 TO -0.064 | 0 |
| -0.064 TO -0.062 | 0 |
| -0.062 TO -0.060 | 0 |
| -0.060 TO -0.058 | 0 |
| -0.058 TO -0.056 | 0 |
| -0.056 TO -0.054 | 0 |
| -0.054 TO -0.052 | 0 |
| -0.052 TO -0.050 | 0 |
| -0.050 TO -0.048 | 0 |
| -0.048 TO -0.046 | 0 |
| -0.046 TO -0.044 | 0 |
| -0.044 TO -0.042 | 0 |
| -0.042 TO -0.040 | 0 |
| -0.040 TO -0.038 | 0 |
| -0.038 TO -0.036 | 0 |
| -0.036 TO -0.034 | 0 |
| -0.034 TO -0.032 | 0 |
| -0.032 TO -0.030 | 0 |
| -0.030 TO -0.028 | 0 |
| -0.028 TO -0.026 | 0 |
| -0.026 TO -0.024 | 0 |
| -0.024 TO -0.022 | 0 |
| -0.022 TO -0.020 | 0 |
| -0.020 TO -0.018 | 0 |
| -0.018 TO -0.016 | 0 |
| -0.016 TO -0.014 | 0 |
| -0.014 TO -0.012 | 0 |
| -0.012 TO -0.010 | 0 |
| -0.010 TO -0.008 | 0 |
| -0.008 TO -0.006 | 0 |
| -0.006 TO -0.004 | 0 |
| -0.004 TO -0.002 | 0 |
| -0.002 TO 0.000 | 0 |
| GREATERTHAN 0.000 | 0 |

NO 4 OF Y IN CM 1470.000 FT FROM THE TARGET

Figure 13. Beam profiles at the third focus in the horizontal and vertical planes respectively. Two sextupoles are used and the momentum is one-half percent above the central design value.

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5000 RAYS

-26-

2 sexts -~~TM-374~~ (u)

2254.000

| INTERVAL | SCALE FACTOR: 100 X'S EQUAL 316 RAYS |
|-------------------|---|
| LESS THAN -0.200 | 316 XXX |
| -0.190 TO -0.190 | 65 XXXXXXXXXXXXXXXXXXXXXXXXX |
| -0.190 TO -0.182 | 84 XXXXXXXXXXXXXXXXXXXXXXXXX |
| -0.180 TO -0.172 | 86 XXXXXXXXXXXXXXXXX |
| -0.170 TO -0.162 | 77 XXXXXXXXXXXXXXXXX |
| -0.160 TO -0.152 | 95 XXXXXXXXXXXXXXXXX |
| -0.150 TO -0.142 | 88 XXXXXXXXXXXXXXXXX |
| -0.140 TO -0.132 | 113 XXXXXXXXXXXXXXXXX |
| -0.130 TO -0.120 | 102 XXXXXXXXXXXXXXXXX |
| -0.120 TO -0.112 | 124 XXXXXXXXXXXXXXXXX |
| -0.110 TO -0.102 | 135 XXXXXXXXXXXXXXXXX |
| -0.100 TO -0.092 | 106 XXXXXXXXXXXXXXXXX |
| -0.090 TO -0.082 | 112 XXXXXXXXXXXXXXXXX |
| -0.080 TO -0.072 | 131 XXXXXXXXXXXXXXXXX |
| -0.070 TO -0.060 | 121 XXXXXXXXXXXXXXXXX |
| -0.060 TO -0.050 | 137 XXXXXXXXXXXXXXXXX |
| -0.050 TO -0.040 | 129 XXXXXXXXXXXXXXXXX |
| -0.040 TO -0.030 | 129 XXXXXXXXXXXXXXXXX |
| -0.030 TO -0.020 | 116 XXXXXXXX |
| -0.020 TO -0.010 | 125 XXXXXXXXXXXXXXXXX |
| -0.010 TO 0.010 | 112 XXXXXXXXXXXXXXXXX |
| 0.010 TO 0.020 | 132 XXXXXXXXXXXXXXXXX |
| 0.020 TO 0.030 | 146 XXXXXXXXXXXXXXXXX |
| 0.030 TO 0.040 | 133 XXXXXXXXXXXXXXXXX |
| 0.040 TO 0.050 | 135 XXXXXXXXXXXXXXXXX |
| 0.050 TO 0.060 | 113 XXXXXXXXXXXXXXXXX |
| 0.060 TO 0.070 | 123 XXXXXXXXXXXXXXXXX |
| 0.070 TO 0.080 | 117 XXXXXXXXXXXXXXXXX |
| 0.080 TO 0.090 | 137 XXXXXXXXXXXXXXXXX |
| 0.090 TO 0.100 | 125 XXXXXXXXXXXXXXXXX |
| 0.100 TO 0.110 | 95 XXXXXXXXXXXXXXXXX |
| 0.110 TO 0.120 | 122 XXXXXXXXXXXXXXXXX |
| 0.120 TO 0.130 | 122 XXXXXXXXXXXXXXXXX |
| 0.130 TO 0.140 | 109 XXXXXXXXXXXXXXXXX |
| 0.140 TO 0.150 | 122 XXXXXXXXXXXXXXXXX |
| 0.150 TO 0.160 | 93 XXXXXXXXXXXXXXXXX |
| 0.160 TO 0.170 | 82 XXXXXXXXXXXXXXXXX |
| 0.170 TO 0.180 | 71 XXXXXXXXXXXXXXXXX |
| 0.180 TO 0.190 | 84 XXXXXXXXXXXXXXXXX |
| 0.190 TO 0.200 | 63 XXXXXXXXXXXXXXXXX |
| GREATERTHAN 0.200 | 314 XXXXXXXXXXXXXXXXX |

NO 1 OF Y IN CM 1027.139 FT FROM THE TARGET

(22)

THE FOLLOWING IS A HISTOGRAM OF X FOR 5000 RAYS

| INTERVAL | SCALE FACTOR: 100 X'S EQUAL 481 RAYS |
|-------------------|--------------------------------------|
| LESS THAN -4.600 | 8 |
| -4.600 TO -4.592 | 2 |
| -4.592 TO -4.580 | 0 |
| -4.580 TO -4.572 | 0 |
| -4.572 TO -4.562 | 2 |
| -4.562 TO -4.552 | 0 |
| -4.552 TO -4.540 | 0 |
| -4.540 TO -4.530 | 1 |
| -4.530 TO -4.520 | 9 XX |
| -4.520 TO -4.510 | 11 XX |
| -4.510 TO -4.502 | 19 XXX |
| -4.500 TO -4.492 | 52 XXXXXXXXXX |
| -4.492 TO -4.480 | 92 XXXXXXXXXXXXXXXXX |
| -4.480 TO -4.470 | 154 XXXXXXXXXXXXXXXXX |
| -4.470 TO -4.460 | 244 XXXXXXXXXXXXXXXXX |
| -4.460 TO -4.450 | 283 XXXXXXXXXXXXXXXXX |
| -4.450 TO -4.440 | 333 XXXXXXXXXXXXXXXXX |
| -4.440 TO -4.432 | 358 XXXXXXXXXXXXXXXXX |
| -4.432 TO -4.420 | 431 XXXXXXXXXXXXXXXXX |
| -4.420 TO -4.410 | 378 XXXXXXXXXXXXXXXXX |
| -4.410 TO -4.400 | 377 XXXXXXXXXXXXXXXXX |
| -4.400 TO -4.390 | 368 XXXXXXXXXXXXXXXXX |
| -4.390 TO -4.380 | 375 XXXXXXXXXXXXXXXXX |
| -4.380 TO -4.370 | 392 XXXXXXXXXXXXXXXXX |
| -4.370 TO -4.360 | 327 XXXXXXXXXXXXXXXXX |
| -4.360 TO -4.350 | 239 XXXXXXXXXXXXXXXXX |
| -4.350 TO -4.340 | 262 XXXXXXXXXXXXXXXXX |
| -4.340 TO -4.330 | 165 XXXXXXXXXXXXXXXXX |
| -4.330 TO -4.320 | 74 XXXXXXXXXXXXXXXXX |
| -4.320 TO -4.312 | 21 XXXXX |
| -4.310 TO -4.300 | 8 X |
| -4.300 TO -4.292 | 1 |
| -4.292 TO -4.280 | 2 |
| -4.280 TO -4.270 | 0 |
| -4.270 TO -4.260 | 0 |
| -4.260 TO -4.250 | 2 |
| -4.250 TO -4.240 | 0 |
| -4.240 TO -4.230 | 2 |
| -4.230 TO -4.220 | 0 |
| -4.220 TO -4.210 | 0 |
| -4.210 TO -4.200 | 0 |
| GREATERTHAN 0.200 | 0 |

NO 2 OF X IN CM 1041.139 FT FROM THE TARGET

Figure 14. Beam profiles at the second focus in the vertical and horizontal planes respectively. Two sextupoles are used and the momentum is one percent above the central design value.

THE FOLLOWING IS A HISTOGRAM OF X FOR 5010 RAYS

(23)
-27-

TM-374
2254.000

| INTERVAL | SCALE FACTOR: 120 X'S EQUAL 386 RAYS |
|-------------------|--------------------------------------|
| LESS THAN -0.230 | 0 |
| -0.220 TO -0.190 | 0 |
| -0.190 TO -0.180 | 0 |
| -0.180 TO -0.170 | 0 |
| -0.170 TO -0.160 | 2 |
| -0.160 TO -0.150 | 0 |
| -0.150 TO -0.140 | 0 |
| -0.140 TO -0.130 | 0 |
| -0.130 TO -0.120 | 0 |
| -0.120 TO -0.110 | 0 |
| -0.110 TO -0.100 | 3 |
| -0.100 TO -0.090 | 27 XXXXXX |
| -0.090 TO -0.080 | 67 XXXXXXXXXXXXXXXXXXXXXXX |
| -0.080 TO -0.070 | 122 XXXXXXXXXXXXXXXXXXXXXXX |
| -0.070 TO -0.060 | 127 XXXXXXXXXXXXXXXXXXXXXXX |
| -0.060 TO -0.050 | 154 XXXXXXXXXXXXXXXXXXXXXXX |
| -0.050 TO -0.040 | 197 XXXXXXXXXXXXXXXXXXXXXXX |
| -0.040 TO -0.030 | 265 XXXXXXXXXXXXXXXXXXXXXXX |
| -0.030 TO -0.020 | 323 XXXXXXXXXXXXXXXXXXXXXXX |
| -0.020 TO -0.010 | 364 XXXXXXXXXXXXXXXXXXXXXXX |
| -0.010 TO 0.000 | 369 XXXXXXXXXXXXXXXXXXXXXXX |
| 0.000 TO 0.010 | 386 XXXXXXXXXXXXXXXXXXXXXXX |
| 0.010 TO 0.020 | 367 XXXXXXXXXXXXXXXXXXXXXXX |
| 0.020 TO 0.030 | 380 XXXXXXXXXXXXXXXXXXXXXXX |
| 0.030 TO 0.040 | 365 XXXXXXXXXXXXXXXXXXXXXXX |
| 0.040 TO 0.050 | 343 XXXXXXXXXXXXXXXXXXXXXXX |
| 0.050 TO 0.060 | 304 XXXXXXXXXXXXXXXXXXXXXXX |
| 0.060 TO 0.070 | 266 XXXXXXXXXXXXXXXXXXXXXXX |
| 0.070 TO 0.080 | 213 XXXXXXXXXXXXXXXXXXXXXXX |
| 0.080 TO 0.090 | 151 XXXXXXXXXXXXXXXXXXXXXXX |
| 0.090 TO 0.100 | 112 XXXXXXXXXXXXXXXXXXXXXXX |
| 0.100 TO 0.110 | 76 XXXXXXXXXXXXXXXXXXXXXXX |
| 0.110 TO 0.120 | 34 XXXXXXXX |
| 0.120 TO 0.130 | 5 X |
| 0.130 TO 0.140 | 0 |
| 0.140 TO 0.150 | 0 |
| 0.150 TO 0.160 | 0 |
| 0.160 TO 0.170 | 0 |
| 0.170 TO 0.180 | 0 |
| 0.180 TO 0.190 | 0 |
| 0.190 TO 0.200 | 0 |
| GREATERTHAN 0.200 | 0 |

NO 3 OF X IN CM 1470.000 FT FROM THE TARGET

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5000 RAYS

(24)

| INTERVAL | SCALE FACTOR: 102 X'S EQUAL 192 RAYS |
|-------------------|--------------------------------------|
| LESS THAN -0.230 | 12 XXXXX |
| -0.230 TO -0.190 | 24 XXXXXXXX |
| -0.190 TO -0.180 | 31 XXXXXXXXXXXXXXX |
| -0.180 TO -0.170 | 43 XXXXXXXXXXXXXXX |
| -0.170 TO -0.160 | 64 XXXXXXXXXXXXXXX |
| -0.160 TO -0.150 | 87 XXXXXXXXXXXXXXX |
| -0.150 TO -0.140 | 93 XXXXXXXXXXXXXXX |
| -0.140 TO -0.130 | 95 XXXXXXXXXXXXXXX |
| -0.130 TO -0.120 | 118 XXXXXXXXXXXXXXX |
| -0.120 TO -0.110 | 141 XXXXXXXXXXXXXXX |
| -0.110 TO -0.100 | 141 XXXXXXXXXXXXXXX |
| -0.100 TO -0.090 | 149 XXXXXXXXXXXXXXX |
| -0.090 TO -0.080 | 156 XXXXXXXXXXXXXXX |
| -0.080 TO -0.070 | 145 XXXXXXXXXXXXXXX |
| -0.070 TO -0.060 | 191 XXXXXXXXXXXXXXX |
| -0.060 TO -0.050 | 176 XXXXXXXXXXXXXXX |
| -0.050 TO -0.040 | 151 XXXXXXXXXXXXXXX |
| -0.040 TO -0.030 | 172 XXXXXXXXXXXXXXX |
| -0.030 TO -0.020 | 187 XXXXXXXXXXXXXXX |
| -0.020 TO -0.010 | 192 XXXXXXXXXXXXXXX |
| -0.010 TO 0.000 | 165 XXXXXXXXXXXXXXX |
| 0.000 TO 0.010 | 168 XXXXXXXXXXXXXXX |
| 0.010 TO 0.020 | 171 XXXXXXXXXXXXXXX |
| 0.020 TO 0.030 | 175 XXXXXXXXXXXXXXX |
| 0.030 TO 0.040 | 186 XXXXXXXXXXXXXXX |
| 0.040 TO 0.050 | 177 XXXXXXXXXXXXXXX |
| 0.050 TO 0.060 | 172 XXXXXXXXXXXXXXX |
| 0.060 TO 0.070 | 139 XXXXXXXXXXXXXXX |
| 0.070 TO 0.080 | 155 XXXXXXXXXXXXXXX |
| 0.080 TO 0.090 | 163 XXXXXXXXXXXXXXX |
| 0.090 TO 0.100 | 129 XXXXXXXXXXXXXXX |
| 0.100 TO 0.110 | 128 XXXXXXXXXXXXXXX |
| 0.110 TO 0.120 | 126 XXXXXXXXXXXXXXX |
| 0.120 TO 0.130 | 124 XXXXXXXXXXXXXXX |
| 0.130 TO 0.140 | 121 XXXXXXXXXXXXXXX |
| 0.140 TO 0.150 | 99 XXXXXXXXXXXXXXX |
| 0.150 TO 0.160 | 72 XXXXXXXXXXXXXXX |
| 0.160 TO 0.170 | 66 XXXXXXXXXXXXXXX |
| 0.170 TO 0.180 | 48 XXXXXXXXXXXXXXX |
| 0.180 TO 0.190 | 22 XXXXXXXXXXXXXXX |
| 0.190 TO 0.200 | 27 XXXXXXXX |
| GREATERTHAN 0.200 | 0 |

NO 4 OF Y IN CM 1470.000 FT FROM THE TARGET

Figure 15. Beam profiles at the third focus in the horizontal and vertical planes respectively. Two sextupoles are used and the momentum is one percent above the central design value.

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5000 RAYS

-28-

4 sexts - $\Delta p/p_0 = 0$ (15)

TM-374

2254.000

INTERVAL

SCALE FACTOR: 100 X'S EQUAL 304 RAYS

LESS THAN -0.270 2

| | |
|------------------|-----|
| -2.200 TO -0.190 | 0 |
| -2.190 TO -0.180 | 0 |
| -2.180 TO -0.170 | 2 |
| -2.170 TO -0.160 | 2 |
| -2.160 TO -0.150 | 3 |
| -2.150 TO -0.140 | 6 |
| -2.140 TO -0.130 | 12 |
| -2.130 TO -0.120 | 31 |
| -2.120 TO -0.110 | 41 |
| -2.110 TO -0.100 | 87 |
| -2.100 TO -0.090 | 116 |
| -2.090 TO -0.080 | 164 |
| -2.080 TO -0.070 | 222 |
| -2.070 TO -0.060 | 237 |
| -2.060 TO -0.050 | 230 |
| -2.050 TO -0.040 | 247 |
| -2.040 TO -0.030 | 257 |
| -2.030 TO -0.020 | 291 |
| -2.020 TO -0.010 | 292 |
| -2.010 TO -0.000 | 269 |
| -2.000 TO 0.010 | 304 |
| 0.010 TO 0.020 | 274 |
| 0.020 TO 0.030 | 283 |
| 0.030 TO 0.040 | 272 |
| 0.040 TO 0.050 | 271 |
| 0.050 TO 0.060 | 223 |
| 0.060 TO 0.070 | 233 |
| 0.070 TO 0.080 | 146 |
| 0.080 TO 0.090 | 154 |
| 0.090 TO 0.100 | 123 |
| 0.100 TO 0.110 | 86 |
| 0.110 TO 0.120 | 51 |
| 0.120 TO 0.130 | 16 |
| 0.130 TO 0.140 | 12 |
| 0.140 TO 0.150 | 5 |
| 0.150 TO 0.160 | 1 |
| 0.160 TO 0.170 | 0 |
| 0.170 TO 0.180 | 0 |
| 0.180 TO 0.190 | 2 |
| 0.190 TO 0.200 | 0 |

GREATER THAN 0.200 2

NO 1 OF Y IN CM 1027.139 FT FROM THE TARGET

THE FOLLOWING IS A HISTOGRAM OF X FOR 5000 RAYS

(26)

INTERVAL

SCALE FACTOR: 102 X'S EQUAL 296 RAYS

LESS THAN -0.270

135 XXX

| | | |
|------------------|-----|----------------|
| -2.200 TO -0.190 | 37 | XXXXXXXXXXXX |
| -2.190 TO -0.180 | 31 | XXXXXXXXXXXX |
| -2.180 TO -0.170 | 31 | XXXXXXXXXXXX |
| -2.170 TO -0.160 | 39 | XXXXXXXXXXXXXX |
| -2.160 TO -0.150 | 38 | XXXXXXXXXXXXXX |
| -2.150 TO -0.140 | 41 | XXXXXXXXXXXXXX |
| -2.140 TO -0.130 | 42 | XXXXXXXXXXXXXX |
| -2.130 TO -0.120 | 57 | XXXXXXXXXXXXXX |
| -2.120 TO -0.110 | 59 | XXXXXXXXXXXXXX |
| -2.110 TO -0.100 | 66 | XXXXXXXXXXXXXX |
| -2.100 TO -0.090 | 69 | XXXXXXXXXXXXXX |
| -2.090 TO -0.080 | 94 | XXXXXXXXXXXXXX |
| -2.080 TO -0.070 | 149 | XXXXXXXXXXXXXX |
| -2.070 TO -0.060 | 163 | XXXXXXXXXXXXXX |
| -2.060 TO -0.050 | 174 | XXXXXXXXXXXXXX |
| -2.050 TO -0.040 | 222 | XXXXXXXXXXXXXX |
| -2.040 TO -0.030 | 242 | XXXXXXXXXXXXXX |
| -2.030 TO -0.020 | 246 | XXXXXXXXXXXXXX |
| -2.020 TO -0.010 | 295 | XXXXXXXXXXXXXX |
| -2.010 TO 0.000 | 286 | XXXXXXXXXXXXXX |
| 0.010 TO 0.020 | 244 | XXXXXXXXXXXXXX |
| 0.020 TO 0.030 | 257 | XXXXXXXXXXXXXX |
| 0.030 TO 0.040 | 262 | XXXXXXXXXXXXXX |
| 0.040 TO 0.050 | 241 | XXXXXXXXXXXXXX |
| 0.050 TO 0.060 | 239 | XXXXXXXXXXXXXX |
| 0.060 TO 0.070 | 194 | XXXXXXXXXXXXXX |
| 0.070 TO 0.080 | 176 | XXXXXXXXXXXXXX |
| 0.080 TO 0.090 | 136 | XXXXXXXXXXXXXX |
| 0.090 TO 0.100 | 110 | XXXXXXXXXXXXXX |
| 0.100 TO 0.110 | 73 | XXXXXXXXXXXXXX |
| 0.110 TO 0.120 | 74 | XXXXXXXXXXXXXX |
| 0.120 TO 0.130 | 59 | XXXXXXXXXXXXXX |
| 0.130 TO 0.140 | 69 | XXXXXXXXXXXXXX |
| 0.140 TO 0.150 | 53 | XXXXXXXXXXXXXX |
| 0.150 TO 0.160 | 34 | XXXXXXXXXXXX |
| 0.160 TO 0.170 | 32 | XXXXXXXXXXXX |
| 0.170 TO 0.180 | 28 | XXXXXXXXXX |
| 0.180 TO 0.190 | 24 | XXXXXXXXXX |
| 0.190 TO 0.200 | 31 | XXXXXXXXXX |

GREATER THAN 0.270

173 XXX

NO 2 OF X IN CM 1041.139 FT FROM THE TARGET

Figure 16. Beam profiles at the second focus in the vertical and horizontal planes respectively. Four sextupoles are used and the momentum is the central design value.

THE FOLLOWING IS A HISTOGRAM OF X FOR 5000 RAYS

-29-

TM-574
2254.000

| INTERVAL | SCALE FACTOR: 100 X'S EQUAL 294 RAYS |
|-------------------|---|
| LESS THAN -0.200 | 173 XXX |
| -0.200 TO -0.190 | 37 XXXXXXXXXX |
| -0.190 TO -0.180 | 31 XXXXXXXXXX |
| -0.180 TO -0.170 | 26 XXXXXXXX |
| -0.170 TO -0.160 | 24 XXXXXXXX |
| -0.160 TO -0.150 | 29 XXXXXXXX |
| -0.150 TO -0.140 | 35 XXXXXXXXXX |
| -0.140 TO -0.130 | 57 XXXXXXXXXXXXXXXXX |
| -0.130 TO -0.120 | 69 XXXXXXXXXXXXXXXXX |
| -0.120 TO -0.110 | 57 XXXXXXXXXXXXXXXXX |
| -0.110 TO -0.100 | 73 XXXXXXXXXXXXXXXXX |
| -0.100 TO -0.090 | 73 XXXXXXXXXXXXXXXXX |
| -0.090 TO -0.080 | 111 XXXXXXXXXXXXXXXXX |
| -0.080 TO -0.070 | 139 XXXXXXXXXXXXXXXXX |
| -0.070 TO -0.060 | 172 XXXXXXXXXXXXXXXXX |
| -0.060 TO -0.050 | 196 XXXXXXXXXXXXXXXXX |
| -0.050 TO -0.040 | 238 XXXXXXXXXXXXXXXXX |
| -0.040 TO -0.030 | 238 XXXXXXXXXXXXXXXXX |
| -0.030 TO -0.020 | 261 XXXXXXXXXXXXXXXXX |
| -0.020 TO -0.010 | 254 XXXXXXXXXXXXXXXXX |
| -0.010 TO 0.000 | 242 XXXXXXXXXXXXXXXXX |
| 0.000 TO 0.010 | 287 XXXXXXXXXXXXXXXXX |
| 0.010 TO 0.020 | 294 XXXXXXXXXXXXXXXXX |
| 0.020 TO 0.030 | 246 XXXXXXXXXXXXXXXXX |
| 0.030 TO 0.040 | 244 XXXXXXXXXXXXXXXXX |
| 0.040 TO 0.050 | 217 XXXXXXXXXXXXXXXXX |
| 0.050 TO 0.060 | 171 XXXXXXXXXXXXXXXXX |
| 0.060 TO 0.070 | 167 XXXXXXXXXXXXXXXXX |
| 0.070 TO 0.080 | 179 XXXXXXXXXXXXXXXXX |
| 0.080 TO 0.090 | 97 XXXXXXXXXXXXXXXXX |
| 0.090 TO 0.100 | 71 XXXXXXXXXXXXXXXXX |
| 0.100 TO 0.110 | 63 XXXXXXXXXXXXXXXXX |
| 0.110 TO 0.120 | 61 XXXXXXXXXXXXXXXXX |
| 0.120 TO 0.130 | 57 XXXXXXXXXXXXXXXXX |
| 0.130 TO 0.140 | 42 XXXXXXXXXXXXXXXXX |
| 0.140 TO 0.150 | 38 XXXXXXXXXXXXXXXXX |
| 0.150 TO 0.160 | 44 XXXXXXXXXXXXXXXXX |
| 0.160 TO 0.170 | 42 XXXXXXXXXXXXXXXXX |
| 0.170 TO 0.180 | 37 XXXXXXXXXXXXXXXXX |
| 0.180 TO 0.190 | 32 XXXXXXXXXXXXXXXXX |
| 0.190 TO 0.200 | 31 XXXXXXXXXXXXXXXXX |
| GREATERTHAN 0.200 | 136 XXXXXXXXXXXXXXXXX |

NO 3 OF X IN CM 1472.000 FT FROM THE TARGET

(18)

THE FOLLOWING IS A HISTOGRAM OF Y FOR 5000 RAYS

| INTERVAL | SCALE FACTOR: 100 Y'S EQUAL 477 RAYS |
|-------------------|--------------------------------------|
| LESS THAN -0.200 | 2 |
| -0.200 TO -0.190 | 7 |
| -0.190 TO -0.180 | 2 |
| -0.180 TO -0.170 | 0 |
| -0.170 TO -0.160 | 0 |
| -0.160 TO -0.150 | 0 |
| -0.150 TO -0.140 | 0 |
| -0.140 TO -0.130 | 0 |
| -0.130 TO -0.120 | 2 |
| -0.120 TO -0.110 | 0 |
| -0.110 TO -0.100 | 2 |
| -0.100 TO -0.090 | 1 |
| -0.090 TO -0.080 | 15 XXX |
| -0.080 TO -0.070 | 47 XXXXXXXX |
| -0.070 TO -0.060 | 142 XXXXXXXXXXXXXXXXX |
| -0.060 TO -0.050 | 233 XXXXXXXXXXXXXXXXX |
| -0.050 TO -0.040 | 314 XXXXXXXXXXXXXXXXX |
| -0.040 TO -0.030 | 382 XXXXXXXXXXXXXXXXX |
| -0.030 TO -0.020 | 442 XXXXXXXXXXXXXXXXX |
| -0.020 TO -0.010 | 444 XXXXXXXXXXXXXXXXX |
| -0.010 TO -0.000 | 477 XXXXXXXXXXXXXXXXX |
| 0.000 TO 0.010 | 463 XXXXXXXXXXXXXXXXX |
| 0.010 TO 0.020 | 455 XXXXXXXXXXXXXXXXX |
| 0.020 TO 0.030 | 394 XXXXXXXXXXXXXXXXX |
| 0.030 TO 0.040 | 378 XXXXXXXXXXXXXXXXX |
| 0.040 TO 0.050 | 354 XXXXXXXXXXXXXXXXX |
| 0.050 TO 0.060 | 255 XXXXXXXXXXXXXXXXX |
| 0.060 TO 0.070 | 131 XXXXXXXXXXXXXXXXX |
| 0.070 TO 0.080 | 54 XXXXXXXXXXXXXXXXX |
| 0.080 TO 0.090 | 15 XXX |
| 0.090 TO 0.100 | 6 X |
| 0.100 TO 0.110 | 0 |
| 0.110 TO 0.120 | 0 |
| 0.120 TO 0.130 | 0 |
| 0.130 TO 0.140 | 0 |
| 0.140 TO 0.150 | 0 |
| 0.150 TO 0.160 | 0 |
| 0.160 TO 0.170 | 0 |
| 0.170 TO 0.180 | 2 |
| 0.180 TO 0.190 | 2 |
| 0.190 TO 0.200 | 0 |
| GREATERTHAN 0.200 | 0 |

NO 4 OF Y IN CM 1472.000 FT FROM THE TARGET

Figure 17. Beam profiles at the third focus in the horizontal and vertical planes respectively. Four sextupoles are used and the momentum is the central design value.